

Commercial Shipping Harbour and Fishing Boat Harbour



A summary of Berth Facilities and Capacities at Geraldton Port



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Version	Revision Date	Details	Prepared By	Reviewed By	Authorised By
J	Jan 2020	Removed information duplicated in Aecom Berthing Capacity Assessment 2014 A503432	JH	JR/CS	PD
		Updated Berth 1+2 Capacities as per Aecom Report Jan 2019 A1167678			
		Updated Berth 3 Ext, B4 Rear Cantilever and Berth 5 Load Ratings after MCM Berth Strengthening Works 2018 / 2019			
		Included B4 Shiploader crane location drawing			
		Included B6 LHM280 Crane Location drawings from 12911N Rev C Report A1310733			
		Included B6 Hopper Capacity from D+A Report P0020-R-001 Rev 0 A925725			
		Updated construction details B1-B3 and included additional Original Drawings in Appendix H			
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		Add 4 No. QRHs and 4 x 125T bollards to the eastern end of B4			
		Add 4 No. 125T bollards to southern end of B6 Add new Hopper data to B6			



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1 Introduction, Interpretation and Limitations

This document presents a list of current facilities within the Commercial Shipping Harbour and of some facilities within the Fishing Boat Harbour of the Geraldton Port. It does not address jetties in the Work Boat Base Marina (for example, Tug and Pilot Boat Facilities).

The Wharf Specification Book describes the facilities and their capacities in terms of berthing, mooring and deck loads, as well as providing a list of the equipment on the facilities. Berth 7 is privately owned infrastructure and any information pertaining to this berth should be verified with the owner prior to accessing the site.

Unless indicated otherwise the notional capacities in this book are based on designs. Individual components may be downgraded from time to time because of the prevailing condition of asset components and accordingly the status should always be checked with the Mid West Ports Authority (MWPA) Engineering Department.

In 2018 a Berth Structural Mooring Load Capacity assessment was completed by D+A, reductions in capacity for Berths 3, 4 and 6 were put in place. The load capacity plans in the book depict those reductions from the design capacities.

The book is intended to cover the loading cases as shown on the drawings and any diversion from these should be referred to the Engineer for comment. Also refer to Section 9 for disclaimer information.

No work on berths is permitted other than in accordance with the MWPA 'Permit System'.

MWPA Procedure 4.1 - Permit to Work Procedure indicates that permits are required for any shore based crane lift, vessel based crane lift (other than those vessel-based lifts that are exempt) or the stacking of loads onto a wharf. Land based crane lifts include all lifts when cranes are set up on wharves.

Apart from No Load zones applicable to some areas of Berths, the following uniformly distributed loads (UDL) generally apply to the berths when using vessel based lifts/wharf loading arrangements. (See drawing 009-MA-0011 in Appendix A for more detail).

Table 1 – Wharf UDL Capacities With / Without Vessel Alongside

Berth	UDL (With Vessel Alongside)	UDL (Without Vessel Alongside)
Berth 1	2.5 T/m ²	3.4 T/m ²
Berth 2	2.5 T/m ²	3.4 T/m ²
Berth 3	1.0 T/m ²	5.0 T/m ²
Berth 3 Ext.	0 T/m ²	1.5 T/m²
Berth 4 Ext.	4.5 T/m ²	4.5 T/m ²
Berth 4	1 T/m²	4.5 T/m ²
Berth 5	4.5 T/m ²	4.5 T/m ²
Berth 6	2.0 T/m ²	3.4 T/m², 8.0 T/m² in load out zone

^{*} There is a 0.5T/m² UDL restriction within a 6m wide x 12.2m long exclusion zone around any live bollard (Appendix B 009-MA-0012)

To determine loading capacity on decks current information can be obtained by contacting permits@midwestports.com.au or by contacting the Duty Wharf Supervisor on 0437 413 734. Where there is any doubt about the need for a permit, contact should be made to the number above.



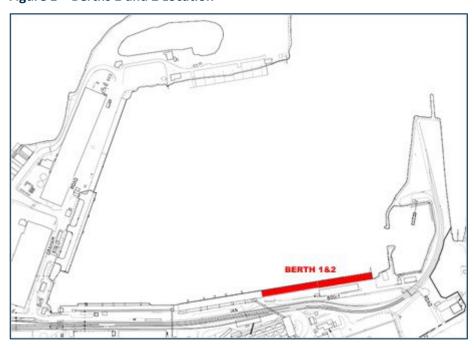
The reference within this book to bollards of capacities at given berths relates to the bollards that are fixed along the length of the wharf or at either adjacent mooring anchor blocks or adjacent mooring dolphins. Note that a vessel positioned at a berth might utilise bollards located at an adjacent wharf. Mooring layouts are at the instruction of the marine pilots and Harbour Master.

All aspects of the Load Capacity Plans must be complied with. These requirements include the following.

- Positioning relative to beams and piles.
- Load exclusion zones for single and multiple bearing loads.
- The nominated loadings are gross loadings, that is, includes the effect of wind, slewing, luffing, and the like.
- The dynamic multiplier for the lifting operation is assumed to be 1.0. Should the dynamic multiplier exceed this the nominated loadings will have to be reduced accordingly (refer to Appendix E).
- Cranes are only operated within the in-service wind conditions as set out in the appropriate Australian Standard.
- No other loads, (including mooring loads), are permitted within 5m from each crane outrigger pad (refer Appendix B).
- Minimum outrigger pad size is 1.2m x 1.2m as shown on the relevant load plan drawing.
- Minimum distance between outrigger pads is 7.0m, centre to centre.
- No ship berthing is to be conducted during lifting operations.
- Authorisation of outrigger load distribution pads by the MWPA engineer is required.

2 Berths 1 and 2

Figure 1 - Berths 1 and 2 Location





Berths 1 and 2 are located at the south-east corner of the Commercial Shipping Harbour in the Port of Geraldton, refer dwg 010-G-0022 in Appendix A.

The combined wharf structure along Berth 1 and Berth 2 is 277.8m, with a deck elevation at the front edge of approximately +3.75m Port Datum (Port Datum = 0.547m below AHD). Be aware that the port datum has changed over time and that older drawings, including some appended to this document, may reflect what at first glance may seem to be different levels.

2.1 DESCRIPTION

The original wharf structure was built around 1931 and included the original Berth 3 wharf. The Berth 1 and 2 wharf were refurbished in 1999/2000 by constructing a new concrete deck on top of the old concrete deck. The new deck was connected to the existing piles by dowels drilled into the top of the piles and 4 no. tie-backs were installed. The old concrete deck and concrete beams are significantly deteriorated and provide very little structural capacity to the deck. In 2018 an additional 24 tie-backs were installed. These anchors supplanted the deteriorated capacity of the existing transverse concrete beams to ensure the global lateral stability of the wharf.

2.2 DECK LOAD CAPACITY

The general deck capacity is:

- No vessel or mooring lines: Uniformly Distributed Load of 3.4 tonne/m² (refer dwg 009-MA-0011 Appendix A);
- Vessel alongside: Uniformly Distributed Load of 2.5 tonne/m2, UDL limited to 0.5tonne/m² within a 6m wide x 12.2m long exclusion zone around any Bollard with a mooring line attached (refer dwg 009-MA-0011 in Appendices A + 009-MA-0012 in Appendix B);
- Wheel Load from a T44 or B-Double Truck (refer Appendix D); and
- Weight of a fully loaded 'Stevens' Hopper. When the Hopper is in use there is to be a minimum 50m separation between the Hopper (and Truck being loaded) to any other truck.

The $1.2 \text{m} \times 1.2 \text{m}$ crane outrigger load capacity of the wharf deck for Berths 1 + 2 is detailed on Drawing No. 009-MA-0012 in Appendix B.

Note: The use of different sized outrigger arrangements will result in different localised vertical loads to those referred to in Appendix 009-MA-0012 in Appendix B. To seek approval for alternative load arrangements, which fall outside the conditions of the wharf load capacity plans provided in 009-MA-0012 in Appendix B, contact the MWPA Engineering Department.

2.2.1 Loading Restriction Clarification

T44 = standard truck load of 44 tonnes (also see dwg 009-MA-0011 in Appendix A):

- Front axle = 4.8 tonnes
- Rear axle = 9.6 tonnes each x 4 axles

B-Double = standard truck load of 62.5 tonnes, 27.5m long (also see Appendix D Table C6.2(C)

- Front axle = 6.0 tonnes
- Tandem axle = 16.5 tonnes
- Triaxle = 20.0 tonnes
- Triaxle= 20.0 Tonnes



Mobile Fertiliser Hopper (Steven's)

- Self-weight of Steven's Hopper (on wheels) = 22 tonnes
- Self-weight of Steven's Hopper + weight of grain inside hopper (on skids) = 135 tonnes
- Two Number skids each of dimensions: 6.73m X 0.64m

2.3 BOLLARD CAPABILITIES

Berths 1 and 2 mooring bollards range in capacity from 20 tonne to 75 tonne. Two inshore bollards located between Berth 2 and Berth 3 have recently been tied back to the deadman anchor, increasing their capacity to 100T each. Mooring bollards are connected to the deck via cast in bolts or chemically anchored threads.

The specific location and capacities of bollards is represented in Appendix C on Drawing 009-MA-0002.

2.4 FENDER DATA

The following fender data applies.

Table 2 - Berth 2 Fender Data

Fender Manufacturer	HS Chemical
Fender Type	Arch
Fender size / designation	NV1000 (1m long)
Rubber Grade	RG100
Rubber Tolerance %	10%
Rated Energy Capacity (kNm) ¹	289
Rated Reaction (kN) ¹	717
Facing Panel size (where applicable)	1.0 h x 0.8 w ²
Fender Manufacturer	HS Chemical

Notes

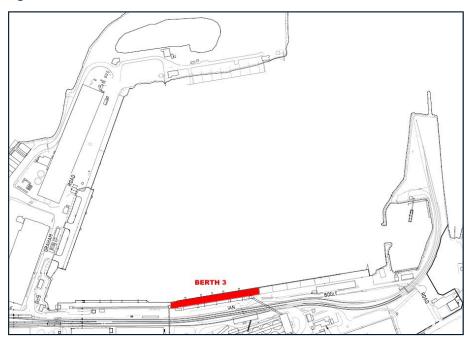
- The manufacturers rated data for energy and reaction must be modified for tolerance, temperature, velocity of compression and angular effects.
- ² No punch fitted dimensions in the face area of the fender.

The above data or rubber compound type and grade has not been independently evaluated, confirmed or tested. Rubber grade is marked on fenders and in all cases is confirmed by historical data from design drawings and/or design reports. The manufacturer's published data is used for the assessment of the fenders.



3 Berth 3

Figure 2 - Berth 3 Location



Berth 3 is located at the southern boundary of the Commercial Shipping Harbour in the Port of Geraldton, refer Appendix A.

The wharf length is 223.4m long, including Berth 3 Extension, with a deck elevation of approximately 3.58m Port Datum (Port Datum = 0.547m below AHD). Be aware that the port datum has changed over time and that older drawings, including some appended to this document, may reflect what at first glance may seem to be different levels.

3.1 DESCRIPTION

The Berth 3 original wharf was built around 1931. It was refurbished in 1996/1997 by driving extra steel piles at mid-span between the existing concrete columns. These steel piles support a 510mm thick reinforced concrete deck constructed on top of the old concrete deck.

The Berth 3 Wharf Extension (circa 1964) is 40.8m long, at the west end of the berth, and consists of a 500mm thick reinforced concrete deck supported by a two-way steel beam system. The primary beams, supported by the steel piles, runs in a north-south direction, or perpendicular to the berth face, and consist of 690UB. The secondary beams run in an east-west direction, or parallel to the berth face, and consist of 690UB. The Berth 3 extension was built as part of the Berth 4 project that was undertaken by the Public Works Department of WA (PWD). At some time during the period 1964 to 1996 some additional secondary beams were added in some parts of the Berth 3 Extension. The Berth 3 extension was partially overtopped as part of the 1996/1997 Berth 3 wharf refurbishment.

In 2003 five free-standing berthing dolphins were added in front of the Berth 3 wharf.



3.2 DECK LOAD CAPACITY

The 1.2m x 1.2m outrigger load capacity of the wharf deck for Berth 3 is detailed on Drawing No. 009- MA-0013 in Appendix B.

As a result of deterioration of sheet pile wall capping beam the zone that is on the landward side of the Berth 3 Wharf Extension rear piles is not permitted for the setup of cranes1.

Note: The use of different sized outrigger arrangements will result in different localised vertical loads to those referred to in 009-MA-0013 in Appendix B. To seek approval for alternative load arrangements, which fall outside the conditions of the berth load capacity plans provided in 009-MA-0013 in Appendix B, contact the Asset and Engineering Department.

3.2.1 Main Deck (that is, east of pile bent 34 only)

The general deck capacity, excluding the Berth 3 extension, is:

- No vessel or mooring lines: Uniformly Distributed Load of 5 tonne/m2 (refer 009-MA-0011 in Appendix A);
- Vessel alongside: Uniformly Distributed Load of 1.0 tonne/m2 (refer 009-MA-0011 in Appendix A);
- Wheel load from T44 Truck (refer Appendix D);
- Wheel load from 60 tonne (gross) forklift;
- Bogie load from Shiploader of 40.0 tonne.

3.2.2 Berth Extension (that is, west of pile bent 34)

Other than for the zone on the landward side of the rear piles, Berth 3 Extension deck capacity is:

- No vessel or mooring lines: Uniformly Distributed Load of 1.5 tonne/m2 (refer 009-MA-0011 in Appendix A);
- Vessel alongside: No Uniformly Distributed Load allowed (refer 009-MA-0011 in Appendix A);
- Wheel load from 10.0 tonne (gross) forklift

As a result of deterioration of the sheet pile wall capping beam, the zone that is on the landward side of the rear piles has the following lesser capacity, except for the 10m of capping beam between TT03 and the amenities building that was repaired in 2019, to allow 10T forklift access.

- Wheel load from T44 Truck (refer Appendix D);
- Wheel load from 3.5 tonne (gross) forklift over rear capping beam.

3.2.3 Berthing Dolphins

The vertical load capacity on the Berth 3 berthing dolphins is generally 70 tonne on most of the dolphin head but is only 12 tonne (on a $1.2 \text{m} \times 1.2 \text{m}$ outrigger pad) for the 1.0 m wide strip that is closest to the wharf.

3.2.4 Conditions

The load capacity plans are based on the following conditions:

- Cranes are only operated within the in-service wind conditions as set out in the appropriate Australian Standard.
- No other loads (including mooring loads) are permitted within 5m from each crane outrigger pad (refer 009-MA-0013 in Appendix B).
- Minimum outrigger pad size is 1.2m x 1.2m as shown on the relevant load plan drawing.



- Minimum distance between outrigger pads is 7.0m, centre to centre.
- The nominated loadings are gross loadings, i.e. includes the effect of wind, slewing, luffing, etc.
- The dynamic multiplier for the lifting operation is assumed to be 1.0. Should the dynamic multiplier exceed this the nominated loadings will have to be reduced accordingly (refer to Appendix E).
- No ship berthing is to be conducted during these lifting operations.

3.2.5 Loading Restriction Clarification (SMEC, 2013)

- T44 = standard truck load of 44 tonnes (also see Appendix D):
 - Front axle = 4.8 tonnes
 - Rear axle = 9.6 tonnes each x 4 axles
- 3.5 t Fork Lift taken as 5.0t self-weight + 3.5 t load distributed as 7.5t on front axle and 1.0t on rear axle.
- 10.0t Fork Lift taken as 16t self-weight + 10.0t load distributed as 24.0t on front axle and 2.0t on rear axle.

3.3 BOLLARD CAPACITIES

3.3.1 Bollard Capacities

Berth 3 mooring bollards range in capacity from 50 tonne to 75 tonne when applying the allowable wharf UDL limitations detailed on Drawing 009-MA-0011 in Appendix A. The five berthing dolphins are each fitted with a bollard and can support a 75 tonne mooring load.

Mooring bollards are connected to the deck via cast in bolts or sleeved bolts through the deck.

The specific location and capacities of bollards is represented in Appendix C on Drawing 009-MA-0003.

3.4 FENDER DATA

Until 2003 the wharf was fitted with 34 No. NV1,000x1,000 – RG100 Arch fenders from Fenders Australia, manufactured by HS Rubber & Automotive Co Ltd of Korea. Some of these items remain bolted to the old wharf face but they are not in use.

In 2003, five berthing dolphins were built and fitted with Fentek SCN 12001.1 fenders (by Trelleborg). The following fender data applies.

Table 3 - Berth

Fender Manufacturer	Fentek
Fender Type	Cone
Fender size / designation	SCN 1200
Rubber Grade	E1.1
Rubber Tolerance %	5%
Rated Energy Capacity (kNm) ¹	688
Rated Reaction (kN) ¹	1073
Facing Panel size (where applicable)	2.67 h x 2.07 w
Fender Manufacturer	Fentek



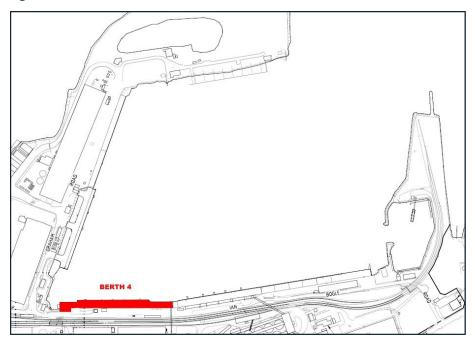
Notes

- The manufacturers rated data for energy and reaction must be modified for tolerance, temperature, velocity of compression and angular effects.
- No punch fitted dimensions in the face area of the fender.

The above data or rubber compound type and grade has not been independently evaluated, confirmed or tested. Rubber grade is marked on fenders and in all cases is confirmed by historical data from design drawings and/or design reports. The manufacturer's published data is used for the assessment of the fenders

4 Berth 4

Figure 3 - Berth 4 Location



Berth 4 is located at the south-west corner of the Commercial Shipping Harbour in the Port of Geraldton, refer Appendix A.

The wharf structure is 282.4m long, including the Berth 4 Extension wharf, with a deck elevation of approximately 3.08m Port Datum (Port Datum = 0.547m below AHD). Be aware that the port datum has changed over time and that older drawings, including some appended to this document, may reflect what at first glance may seem to be different levels.



4.1 DESCRIPTION

Berth 4 Original Wharf (1964) consists of a 181.1m long, 248mm thick reinforced concrete deck with a 115mm thick non-structural topping supported by a two way beam system. The primary beams run in a north-south direction, or perpendicular to the berth face, and consists of 690UB. The secondary beams run in an east-west direction, or parallel to the berth face, and consist of 690UB.

The Berth 4 west end extension wharf (1987) consists of a 101.3m long, 350mm reinforced concrete deck supported by a two way beam system and bracing angle members. The main beams, perpendicular to the wharf face, are 690UB 140. The secondary beams, parallel to the wharf face, are 690UB 140 at some locations and 690UB 125 at other locations.

In 2003, Berth 4 was amended to add five free standing berthing dolphins and "infill" deck sections that are adjacent to and between the berthing dolphins. Berth 4 infill sections consist of a 125mm reinforced concrete topping over 250mm depth pre-stressed concrete planks that are supported by 610UB 125 beams. Relevant typical drawings are in Appendix H.

In 2017 areas of the original wharf and the 1987 extension substructure were strengthened to accommodate increased rail loads from Shiploader 4. Longitudinal beams at the rear of the wharf were increased in depth of section and an additional steel longitudinal beams were introduced near the front of the original deck.

In 2022 the Original Wharf 4 (constructed in 1964) was strengthened further. The strengthening works consisted of a partial demolition of the top of the original deck and the installation of a new reinforced concrete topping, as well as a below deck thickening, increasing the minimum designed deck thickness to 600mm. Further to this, connection between the Newly Strengthen Original Wharf 4 slab and the adjacent infill slabs, and Wharf 4 Extension slab was undertaken. The shears key between Newly Strengthen Original Wharf 4 and Wharf 4 Extension was replaced with additional steel work. An additional Structural Steel deck was added out front at the east end.

4.2 DECK LOAD CAPACITY

4.2.1 Uniformly Distributed Loads (UDL)

The different structures combining to make up Berth 4 have varying allowable deck capacities depending on age, condition and design.

The allowable uniformly distributed load capacities on Berth 4, in combination with vessel loading and in the absence of mooring forces are detailed on Drawing 009-MA-0011 in Appendix A.

4.2.2 Crane Loads

The $1.2 \text{m} \times 1.2 \text{m}$ crane outrigger load capacity of the wharf deck for Berth 4 is detailed on Drawing No. 009-MA-0016 in Appendix B.

Note: The use of different sized outrigger arrangements will result in different localised vertical loads to those referred to in Appendix B. To seek approval for alternative load arrangements, which fall outside the conditions of the berth load capacity plans provided in Appendix B, contact the MWPA Engineering Department.



SHIPLOADER LOADS

The Berth 4 Ship Loader was weighed in January 2019 to assess the Bogie Loads. The full results are in COVA Report 20190214 Report 001 (4710.015) Rev C which is available from the Asset and Engineering Department. Extracted results are tabulated in Figure 6.

Figure 5 - Shiploader 04 - Bogie Loads

Observed Corner, Total Weights and CoG											
			Corner Weight (Tonn					CoG (m	nm)	Con	ditions
Machine Config.	Luff	Shuttle Position	NE	SE	NW	SW	Total Weight (Tonne)	ΔΧ	ΔΥ	Wind Speed (m/s)	Wind Direction
1	+0.4°	Out	111.4	76.3	121.2	65.7	374.6	1610.8	12.81	5 m/s	190°
2	+0.4°	In	106.3	82.0	117.1	69.1	374.4	1287.2	33.66	5 m/s	210°
3	+14.9°	Out	124.1	64.6	124.1	62.9	375.7	2142.4	28.75	5 m/s	190°
4	+14.9°	In	105.9	82.4	115.8	70.3	374.4	1228.4	32.59	5-6 m/s	210°
5	+72.5°	In	82.8	106.3	94.5	90.9	374.7	-348.0	53.85	5-6 m/s	210°
					Average Wei		374.7				

Table 1: Observed Corner Reactions, Total Reactions and CoG

4.2.3 Vehicle Loading

Unless demarcated as a 'No Load' zone on the drawings contained in Appendix B, T44 or B-Double truck loading is permitted on Berth 4.

Allowable forklift loads are as follows:

General - 10 tonne (gross) forklift.

Loading Restriction Clarification (SMEC, 2013)

- T44 = standard truck load of 44 tonnes (also see Appendix D):
 - Front axle = 4.8 tonnes
 - Rear axle = 9.6 tonnes each x 4 axles
- 3.5 t Fork Lift taken as 5.0t self-weight + 3.5 t load distributed as 7.5t on front axle and 1.0t on rear axle.
- 10.0t Fork Lift taken as 16t self-weight + 10.0t load distributed as 24.0t on front axle and 2.0t on rear

The berth 4 Steel seaward deck has been designed for the following loading:

- Forklift Hyundia 7T
- Axle loading (Loaded) Front /Rear: 14564 kg/ 1866kg
- Axle Loading (loaded) Front/Rear 3867kg /5564kg



- Shore Tension System Including:
 - Shore Tension Unit (3200kg)
 - St Bollard (1086kg)
 - Snatch Block (600kg)
 - 5kPa Live Load

4.3 BOLLARD CAPACITIES

Berth 4 mooring bollards range in capacity from 6 tonne to 75 tonne when applying the allowable wharf UDL limitations detailed on Drawing 009-MA-0011 in Appendix A. There are 4 no. 60T dual hook QRH (Quick Release Hooks) installed at the Eastern End of Berth 4. East QRH is fitted with a capstan and the hooks are linked to a remote release console located near the centre of the wharf.

The five berthing dolphins are each fitted with a bollard and can support a 75 tonne mooring load. There are also two 50 tonne (four bolt) bollards on a concrete footing block at the base of Transfer Tower TT502.

There are also 4 x 125T Tee Bollards located at the eastern end of Berth 4.

Mooring bollards are connected to the deck via cast in bolts or sleeved bolts through the deck.

The specific location and capacities of bollards is represented in Appendix C on Drawing 009-MA-0004.

4.4 FENDER DATA

Five berthing dolphins are fitted with Fentek SCN 12001.1 fenders (by Trelleborg). The following fender data applies.

Table 4 - Berth 4 Fender Data

Fender Manufacturer	Fentek
Fender Type	Cone
Fender size / designation	SCN 1200
Rubber Grade	E1.1
Rubber Tolerance %	5%
Rated Energy Capacity (kNm) ¹	688
Rated Reaction (kN) ¹	1073
Facing Panel size (where applicable)	2.67 h x 2.07 w

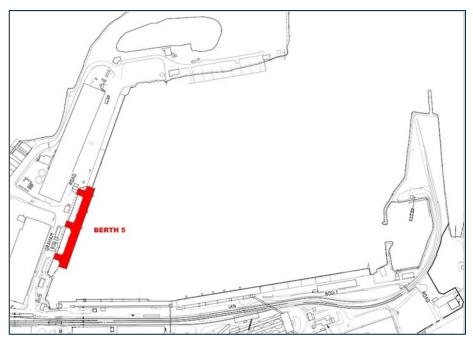
Notes

- ¹ The manufacturers rated data for energy and reaction must be modified for tolerance, temperature, velocity of compression and angular effects.
- No punch fitted dimensions in the face area of the fender.

The above data or rubber compound type and grade has not been independently evaluated, confirmed or tested. Rubber grade is marked on fenders and in all cases is confirmed by historical data from design drawings and/or design reports. The manufacturer's published data is used for the assessment of the fenders.

5 Berth 5

Figure 6 - Berth 5 Location



Berth 5 is located at the Western boundary of the Commercial Shipping Harbour in the Port of Geraldton, refer 009-MA-0011 in Appendix A.

The wharf deck is 213.0m long, with a deck elevation of approximately 3.51m Port Datum (Port Datum = 0.547m below AHD). Be aware that the port datum has changed over time and that older drawings, including some appended to this document, may reflect what at first glance may seem to be different levels.

5.1 DESCRIPTION

The initial Berth 5 consists of a 600mm thick reinforced concrete deck supported by diameter 474mm steel piles. The piles are at a spacing of 4.3m along the face of the berth and 4.9m across the berth.

In 2008, an additional ship loader rail beam, mesh walkways, five berthing dolphins and a shiploader maintenance platform deck were fitted in front of the initial berth deck. The maintenance platform consists of a 225-265mm thick in situ reinforced concrete deck on top of 300m depth precast reinforced concrete planks that are supported by 800 x 400mm fabricated box girders.

5.2 DECK LOAD CAPACITY

5.2.1 Uniformly Distributed Loads (UDL)

The allowable uniformly distributed load capacities for Berth 5 are detailed on Drawing 009-MA-0011 in Appendix A.

The UDL capacity of the Berth 5 deck is:

- No vessel or mooring lines: Uniformly Distributed Load of 4.5 tonne/m2 (refer 009-MA-0011 in Appendix A).
- Vessel alongside: Uniformly Distributed Load of 4.5 tonne/m2 (refer 009-MA-0011 in Appendix A).



5.2.2 Crane Loads

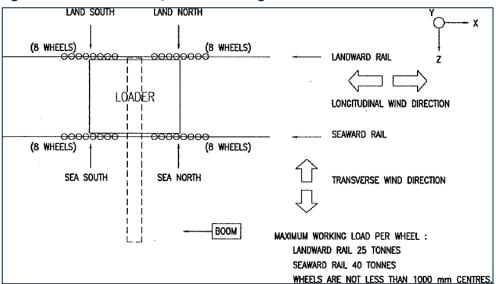
The $1.2m \times 1.2m$ crane outrigger load capacity of the wharf deck for Berth 5 is detailed on Drawing No. 009-MA-0018 in Appendix B.

Note: The use of different sized outrigger arrangements will result in different localised vertical loads to those referred to in Appendix B. To seek approval for alternative load arrangements, which fall outside the conditions of the berth load capacity plans provided in Appendix B, contact the MWPA Engineering Department.

5.2.3 Shiploader Loads

Bogie load from Shiploader 05 of 60.0 tonne or for multiple wheel sets in accordance with Drawing No. 75309405-3541.

Figure 7: Source: Maunsell/Aecom Drawing No. 75309405-3541 Rev 1



5.2.4 Vehicle Loading

The allowable fork lift loading on Berth 5 is as follows:

General: 60T gross fork lift

Loading Restriction Clarification (SMEC, 2013):

- T44 = standard truck load of 44 tonnes (also see Appendix D):
 - Front axle = 4.8 tonnes
 - Rear axle = 9.6 tonnes each x 4 axles

5.3 BOLLARD CAPACITIES

Berth 5 mooring bollards range in capacity from 50 tonne to 75 tonne when applying the allowable wharf UDL limitations detailed on Drawing 009-MA-0011 in Appendix A. The five berthing dolphins are each fitted with a bollard and can support a 75 tonne mooring load. There are also two 75 tonne bollards on stand-alone structures situated to the south of Berth 5.

Mooring bollards on the original deck are connected to the deck via cast in bolts or sleeved bolts through the deck.

The specific location and capacities of bollards is represented in Appendix C on Drawing 009-MA-0005.



5.4 FENDER DATA

No. 5 Berth berthing dolphins are fitted with Fentek SCN 1200 E1.1 fenders (by Trelleborg). The following fender data applies.

Table 5 - Berth 5 Fender Data

Fender Manufacturer	Trelleborg
Fender Type	Cone
Fender size / designation	SCN 1200
Rubber Grade	E1.1
Rubber Tolerance %	5%
Rated Energy Capacity (kNm) ¹	688
Rated Reaction (kN) ¹	1073
Facing Panel size (where applicable)	2.67 h x 2.07 w

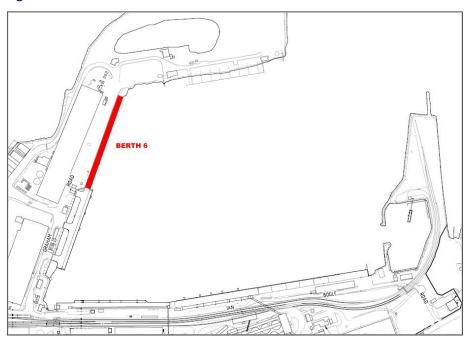
Notes

- ¹ The manufacturers rated data for energy and reaction must be modified for tolerance, temperature, velocity of compression and angular effects.
- No punch fitted dimensions in the face area of the fender.

The above data or rubber compound type and grade has not been independently evaluated, confirmed or tested. Rubber grade is marked on fenders and in all cases is confirmed by historical data from design drawings and/or design reports. The manufacturer's published data is used for the assessment of the fenders.

6 Berth 6

Figure 8 - Berth 6 Location Plan





Berth 6 is located at the north-west corner of the Commercial Shipping Harbour in the Port of Geraldton, refer Appendix 009-MA-0011 in A.

The berth wharf is 245.6m long with a deck elevation of approximately 3.51*m Port Datum (Port Datum = 0.547m below AHD). Be aware that the port datum has changed over time and that older drawings, including some appended to this document, may reflect what at first glance may seem to be different levels.

6.1 DESCRIPTION

Berth 6 was constructed in 1996. It consists of a reinforced concrete deck supported by steel beams. The steel beams run in an east-west direction, or perpendicular to the berth face, and consist of 460UB. The concrete deck consists of 200mm thick precast panels with a 100mm thick in situ concrete pour. Within the loadout bridge the pile and beam spacing is closer than in the remainder of the wharf.

In 1997 a grouted revetment protection mattress was installed under the wharf.

In 2003 a berth pocket was dug (by dipper dredge) along 215m of the length of the face of Berth 6. The pocket is very close to the original front wharf piles, and so a concept was adopted that involved the following components and is depicted on the Drawing No. 49915-DPE-443, Berth 6 Retaining Piles - Typical Section:* From December 2019 Bathymetry Survey, previously 3.50m PD

- A continuous hit-and-miss row of several hundred submerged retaining piles (both round hollow tube and 310UCs) driven under the bolt on vertical concrete drop panels at the wharf face.
- A section of plate is chained between the submerged retaining piles at various locations where a slightly larger gap otherwise exists.
- 15 No. 'fender piles' between the rubber fenders (to protect the most easterly submerged retaining piles).
- Steel mounting frames to stand-off the rubber fenders a nominal dimension of 630mm from the concrete wharf face.
- Excavation by a dipper dredge between the cutter dredging of Jan de Nul and the submerged retaining pile line (fender line).

Pile driving conditions resulted in non-verticality of some of the submerged retaining piles. Those piles which inclined such that the top edge was on the basin side of the fender pile line were either removed or cut off. A number of slightly inclined piles that have been left in place have flat sides encroaching marginally into the nominal berth pocket.

There are approximately 15 No. 610mm dia steel piles spread along the wharf cope line and outside of the concrete face drop panels. Some drawings of the berth refer to the piles as "Fender Piles". The piles sit behind the seaward edge of the fenders and are not intended to provide a fendering function. The piles were installed to cover the tops of the submerged retaining wall piles that encroach closest to the edge of the berth pocket. The top of the exposed piles are secured to the berth face drop panels, and the bottoms of the piles were generally dropped over the top of the driven retaining wall 310 UC piles.



6.2 DECK LOAD CAPACITY

6.2.1 Uniformly Distributed Loads (UDL)

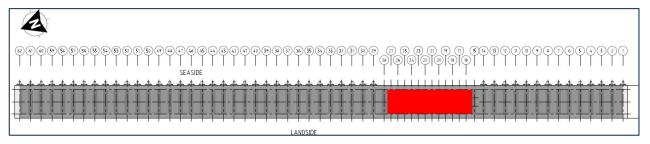
The allowable uniformly distributed load capacities for Berth 6 are detailed on Drawing 009-MA-0011 in Appendix A.

In general, the UDL capacity of the Berth 6 deck is:

- No vessel or mooring lines:
 - Main Deck Uniformly Distributed Load of 3.4 tonne/m2 (refer 009-MA-0011 in Appendix A)
 - Loadout Bridge Uniformly Distributed Load of 8 tonne/m2 (refer 009-MA-0011 in Appendix A)
- Vessel alongside: Uniformly Distributed Load of 2 tonne/m2 (refer 009-MA-0011 in Appendix A).

The capacity of the section of deck between grid lines '15' and '28' (referred to as the Loadout Bridge) is higher by design to facilitate the handling of heavier loads.

Figure 9 - Berth 6 Showing Heavy Load Area



6.2.2 Crane Loads

The 1.2m x 1.2m crane outrigger load capacity of the wharf deck for Berth 6 is detailed on Drawing No. 009-MA-0020 in Appendix B. The heavy loadout section of Berth 6 can support outrigger loads up to 85tonne on a $1.2m \times 1.2m$ crane outrigger pad.

There are Crane specific drawings for the QUBE Liebherr LHM 280 in Appendix B. QUBE has procured a second crane in August 2024. An operating procure was approved for use and the report QUBE Second Crane Aug2024 (A2184672) is available on request.



Note: The use of different sized outrigger arrangements will result in different localised vertical loads to those referred to in Appendix B. To seek approval for alternative load arrangements, which fall outside the conditions of the berth load capacity plans provided in Appendix B, contact the MWPA Engineering Department.



6.2.3 Vehicle Loading

Berth 6 can support a currently legal fully laden B-double truck. Reference is made to table C6.2(C) in AS5100.2.

Figure 10 – Commentary to AS5100.2 Table C6.2(C) B-Double Loading Configuration

TABLE C6.2(C) CURRENT LENGTH VEHICLES—CURRENT FREIGHT DENSITY = 0.28 t/m^3						
O/A length (m)	Gross mass (tonnes)	Configuration, axle distances and axle group mass (see Note)				
25.0	62.5	0 1.6 m	00 5.6 m	000 13.6 m	000 22.6 m	
	O/A length (m)	O/A length (tonnes)	O/A length (tonnes) C	O/A length (m) Gross mass (tonnes) Configuration 25.0 62.5 1.6 m 5.6 m	O/A length (m) Gross mass (tonnes) Configuration, axle di (s 0 00 000 25.0 62.5 1.6 m 5.6 m 13.6 m	O/A length (m) Gross mass (tonnes) Configuration, axle distances and ax (see Note) 0 00 000 000 25.0 62.5 1.6 m 5.6 m 13.6 m 22.6 m

6.2.4 Mobile Fertiliser Hopper (Steven's)

Mid West Ports Authority commissioned Design and Analysis to assess the existing Berth 6 wharf structure with the aim of verifying the capacity of the structure against the loads imposed by the mobile CSL hopper (unloading Heavy Metal Concentrate (HMC). The full results are in D&A Report Berth 6 CSL Hopper Berth Capacity Assessment P0063-R-002 rev 0 which is available from the Asset and Engineering Department.

Below is a summary of the findings of the report and are detailed on Drawing 009-MA-0061 in Appendix B.

- The use of the CSL Hopper between 1 to 16 (inclusive) and 27 to 62 (inclusive) is therefore not recommended.
- For the AS3774 compliant load case the CSL hopper is to only be utilised between bents 16 to 27 (inclusive).
- The hopper should not be positioned within 2 spans, or bays, from a bollard which is being utilised for the mooring of a vessel.
- Hopper skids to be placed no closer than 2m from the seaward edge of the wharf.
- Hopper skids to be positioned parallel with the seaward edge of the wharf.
- Hoppers to be empty during transportation.
- Only a single B-Double or single B-triple is allowed on the berth for the CSL hopper.
- If not unloading, the B-doubles/B-triple should traverse the berth at a maximum
- distance possible away from the hopper location. Trucks and vehicles waiting to be
- loaded must be parked landside off the deck and can only access the deck once the
- newly filled truck has left the berth deck completely.
- MWPA OH&S policies and procedures must be adhered to at all times

The following conditions are applicable during the handling of fertiliser product (0.7t/m3-1.0t/m3)) with the hoppers.

- The hopper should not be positioned within 13m of a bollard which is being used to moor the vessel.
- The hoppers are not to be spaced closer than 20 metres of each other along the length of the berth.



- Hopper skids to be placed no closer than 1.5m from the seaward edge of the berth and 1.6m from the rear of the berth. (seaward edge of berth does not include the concrete panel on berth face)
- Hoppers to be empty during transportation.
- Only a single B-Double is allowed on the berth per hopper.
- If not unloading, the B-doubles should traverse the berth at a maximum distance possible away from the hopper location. Trucks and vehicles waiting to be loaded must be parked landside off the deck and can only access the deck once the newly filled truck has left the berth deck completely

6.3 BOLLARD CAPACITIES

Berth 6 deck-mounted mooring bollards have a 50 -75 tonne capacity when applying the allowable wharf UDL limitations detailed on Drawing 009-MA-0011 in Appendix A. There are also two 75 tonne bollards on mass concrete structures situated to the north of Berth 6 and two inshore 75 tonne bollards at the back of the berth. 4 no. 125T bollards were install in 2024 at the southern end of Berth 6 inshore next to TT503.

Mooring bollards are connected to the deck via sleeved bolts through the deck.

The specific location and capacities of bollards is represented in Appendix C on Drawing 009-MA-0006.

6.4 FENDER DATA

The wharf is fitted with fenders of a number of types and sizes. The rubber fender units are mounted on steel packer frames. The berth is fitted with six no. SM-600H 2500 from Bridgestone – these are mounted vertically (nominal length 2.500m). The berth is also fitted with 54 No. DA A600H (ME) Arch fenders from Bridgestone – these are mounted horizontally (nominal length 1.000m).

Table 6 - Berth 6 Fender Data

Fender Manufacturer	Bridgestone
Fender Type	Arch
Fender size / designation	DA 600 (1.3m long)
Rubber Grade	ME
Rubber Tolerance %	10%
Rated Energy Capacity (kNm) ¹	162
Rated Reaction (kN) ¹	645
Facing Panel size (where applicable)	0.45 h x 1.0 w ²

Notes

- ¹ The manufacturers rated data for energy and reaction must be modified for tolerance, temperature, velocity of compression and angular effects.
- ² No punch fitted dimensions in the face area of the fender.

The above data or rubber compound type and grade has not been independently evaluated, confirmed or tested. Rubber grade is marked on fenders and in all cases is confirmed by historical data from design drawings and/or design reports. The manufacturer's published data is used for the assessment of the fenders.



7 Berth 7

Berth 7 is a privately owned facility any information pertaining to Berth 7 should be verified with the owners.

7.1 MOORING

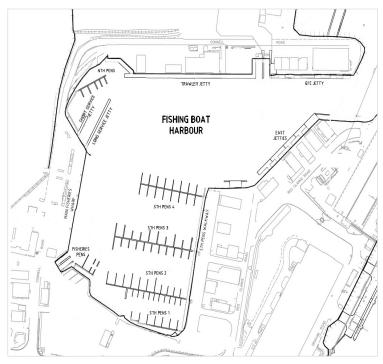
Berth 7 commenced operational services in October 2012 for Panamax Iron Ore vessels port side alongside. It is fitted with a combined mooring line and MoorMaster vacuum mooring system (www.moormaster.com/). The MoorMaster system is not often utilised. The current mooring line plan requires six headlines and six stern lines*.

*Appendix 1 General Mooring Arrangement - Karara Mooring Procedures Berth 7 Rev 3 Aug 2019

8 Fishing Boat Harbour

The layout of the Fishing Boat Harbour and the location of the key components are shown on the Port Infrastructure, Features, Services and Facilities Identification Map in Appendix A.

Figure 11 - Fishing Boat Harbour General Arrangement



Maximum permitted vessel size is 35 metres LOA at maximum draft of 3.5³ metres. For vessels operating at drafts in excess of 3.2 metres tidal information is available from the Harbour Master. North Pens & Access Walkway and the Short Service Jetty has a maximum permitted vessel size of 11m and 2.3m draft.

Entry and departure drafts in the Fishing Boat Harbour Channel are in the range of 3.1 metres to

3.8³ metres accessible up to MSL (Mean Sea Level). Drafts over 3.5³ metres require the written permission of the Harbour Master.

Permission to berth is required from the MWPA, particularly for large vessels. No double banking of vessels on any Fishing Boat Harbour pens, jetties or wharfs is permitted without prior approval from the Trade Team.

https://www.midwestports.com.au/trade/trade.aspx

³ Subject to review and change from time to time.



8.1 MOORING PENS

At present, 152 pens are situated along the north-west, south and south east side of the Fishing Boat Harbour. These pens will generally accommodate boats from 8 to 23 metres overall, with a draft not exceeding 3.5 metres ⁴.

8.2 LONG SERVICE JETTY

The Long Service Jetty is located north of the Main Fishermen's Wharf in the North West area of the Fishing Boat Harbour. The Long Service Jetty was originally constructed circa 1977. This jetty was refurbished in 2017 by an external party to serve as a berthing facility for a tourism vessel and is currently operated under a licence. No access is permitted without prior approval from the licensee.

8.3 MAIN FISHERMEN'S WHARF

The Main Fishermen's Wharf is approximately 155 metres in length and is often referred to as the "fuel berth". Depths of water alongside the facilities vary from 1.5 metres to in excess of 4 metres. The Main Fisherman's Wharf can be divided into two distinct sections, a northern section and a southern section. Note that two of the existing fuel bowsers are located on the southern section and two are located on the northern section which also houses a Crane Lift Zone (approximately centred around Fuel Bowser No. 4 on Figure 13).

The original sheet piled wharf of the Fishing Boat Harbour (FBH) was rehabilitated circa 2000. The rehabilitation project involved the original northern 95m of wall (distinguishable by a notable kink in the face of the wharf). The rehabilitation design provided provision for a -4m seabed level but no more (based on the Chart Datum 0=0.847m below AHD current at the time). The wharf is fendered with timber chafers that are approximately four metres long. The fendering was designed for a maximum normal berthing velocity of 0.3m/sec and an abnormal berthing velocity of 0.4m/sec. The southern 60m of wall was not part of the 2000 rehabilitation project.

In 2019 the entire 155m sheet wall length was repaired and repainted.

8.3.1 Northern Section

The specified maximum allowable safe working loads (SWL) and limitations of the Main Fisherman's Wharf, northern section are as follows:

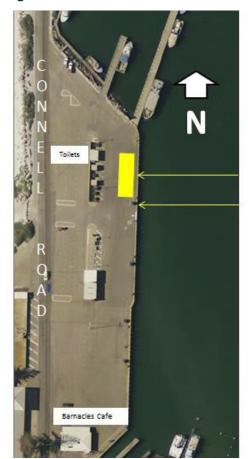
- Crane SWL 20T Max Outrigger Load (3m from wharf edge) within dedicated crane lift zone
- Vessel SWL 400T Trawler Vessel
- Truck SWL 10T Axle Load
- Forklift SWL 10T (1m from wharf edge)
- Wharf UDL 2400kg per m² (1m from wharf edge)

⁴ Subject to review and change from time to time.



The rehabilitated structure is designed for a mobile crane that is capable of lifting 20 tonnes at a radius of 10 metres. Crane set up is only permitted in the crane lift zone that is depicted in Figure 13. For all crane lifts requirements on the wharf outside of this zone prior approval must be obtained from MWPA.

Figure 12 - Crane Lift Zone



CRANE LIFT ZONE

FUEL BOWSER #4

NOTES:

- LIFT ZONE AS PAINTED ON HARDSTAND
 AREA
- 2. MINIMUM 2 METRES FROM FUEL BOWSERS
- 3. MINIMUM 3 METRES FROM WHARF EDGE

8.3.2 Southern Section

The specified maximum allowable safe working loads (SWL) and limitations of the Main Fisherman's Wharf, southern section are as follows:

- Crane SWL No Cranes
- Vessel SWL 200T Trawler Vessel
- Truck SWL 10T Axle Load
- Forklift SWL 10T (1m from wharf edge)
- Wharf UDL 1000kg per m2 (1m from wharf edge)



8.4 OTHER FBH JETTIES

8.4.1 Vertical Loads

Following are the recommended operational restrictions for deck loading.

TRAWLER JETTY

Max loading of 800kg/m².

This Jetty is privately leased and operated by multiple Lessees. Leaseholder consultation needs to occur prior to accessing the area.

GFC JETTY

With reference to Figure 8 below,

- Blue Light vehicle loads only
 2T Fork Lift
- Green Pedestrian Traffic Only

Figure 13 - GFC Jetty Vertical Load Mark-up



This data should be verified with the owners/leaseholders of the facilities before it is used.

8.4.2 Trawler Jetty – Mooring and Berthing Loads

A forensic assessment has been made of a theoretical design vessel for what is now commonly known as the Trawler Jetties that are associated with various lease sites and which were constructed circa 1995.

Before it is used all data should be verified by:

- reading the full reports that are discussed below; and
- consulting the owners / leaseholders of the facilities.

This Jetty is privately leased and operated by multiple Lessees.



9 Disclaimers

The original version of this document and Revisions A to C were produced by Aurecon (previously Connell Wagner). The original Connell Wagner disclaimer is below.

The information contained in this report has been based on the information presented on the drawings issued by the Geraldton Port Authority. It has been assumed that the facilities are in good structural condition and adequately maintained.

Connell Wagner Pty Ltd takes no responsibility for the accuracy of the information presented on the drawings issued by Geraldton Port Authority. Connell Wagner Pty Ltd does not warrant that the drawings reflect the actual structures as constructed. Should the structures deviate from what is shown on the drawings, the impact of this deviation will have to be assessed by a suitably qualified engineer.

Connell Wagner does not warrant the information shown for the drawings for Berth No 1 and 2 as this work was undertaken by Halpern Glick Maunsell.

Many elements of the main body and also within the appendices of the Wharf Specification Book relating to berth or mooring bollard loading capacities were updated based on work undertaken by Design and Analysis (D&A). The following D&A disclaimer applies:

"This Technical Engineering Report has been prepared in accordance with the scope of services agreed upon between D&A and the Mid West Ports Authority (MWPA). To the best of D&A's knowledge, the report presented herein represents the MWPA's intentions at the time of printing of the report. However, the passage of time, manifestation of latent conditions or impacts of future events may result in the actual project and its impact differing from that described in this report. In preparing this report D&A has relied upon data, surveys, analysis, designs, plans and other information provided by MWPA, and other individuals and organisations referenced herein. Except as otherwise stated in this report, D&A has not verified the accuracy or completeness of such data, surveys, analysis, designs, plans and other information.

No responsibility is accepted for use of any part of this report in any other context or for any other purpose by third parties.

This report does not purport to provide legal advice. Readers should engage professional legal advisers for this purpose.

The recommendations presented in this report assumes that the structure is complete and that all remedial works have been completed to degraded elements so as to reinstate their original design capacity. All ongoing strengthening and remedial works affecting the supporting structural system must be completed prior to using the berth structures for the loading arrangements shown in this report. The structural capacity of the structural elements is also assumed to have been maintained in keeping with the details shown on the as- constructed drawings."



10 Monitoring, Evaluation and Review

This document is required to be reviewed every two years from the last scheduled review date.

Minor updates made within this two year period, will not be taken as a *full review*.

The Document Custodian is responsible for conducting the review in accordance with **Controlled Documents Review and Approval Process Work Instruction**.

11 Administration

Document Custodian: Structural Engineer

Document Approver: Assets & Engineering Manager

Approval Date: 29 October 2024

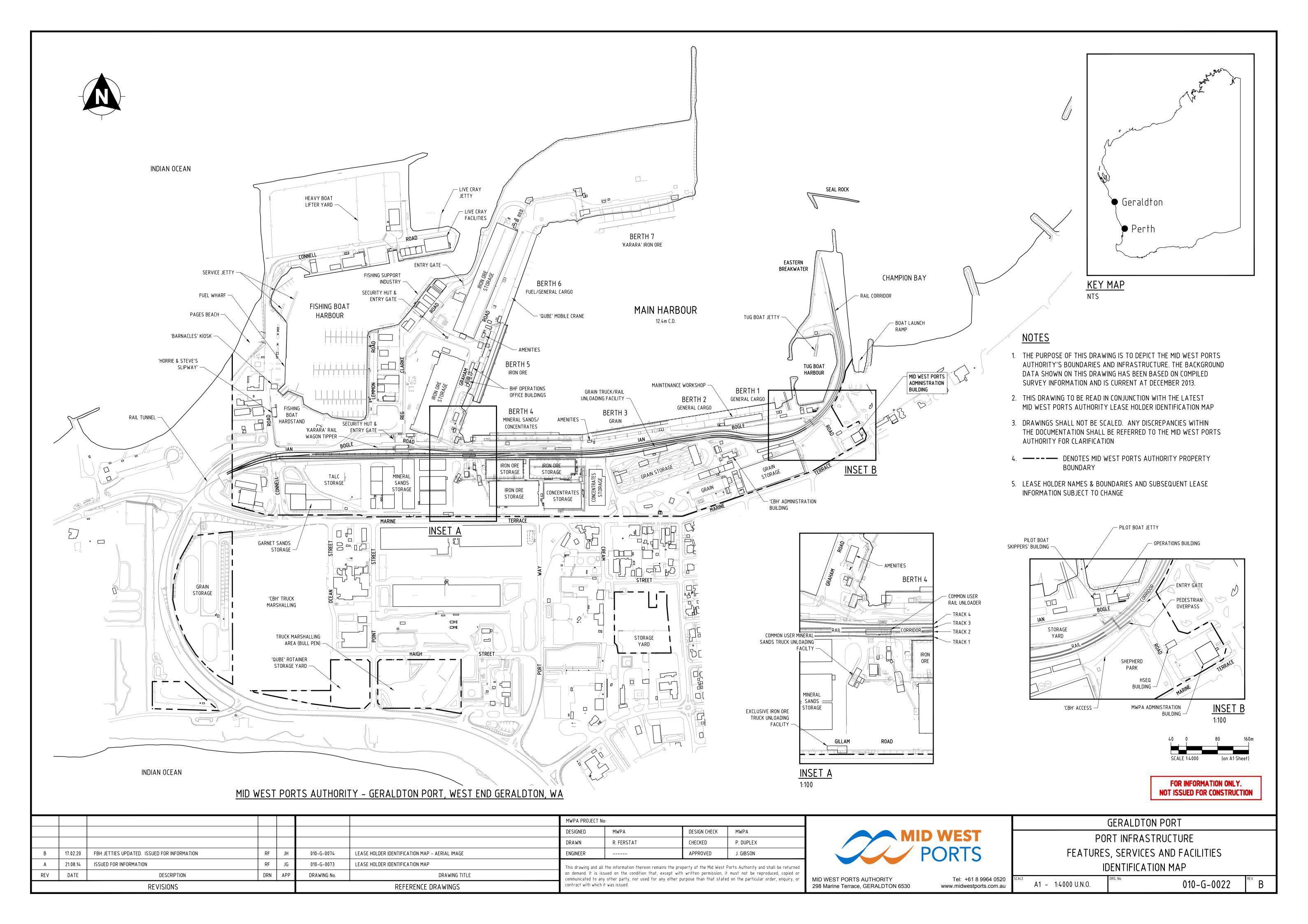
Document Review Period: 2 yrs

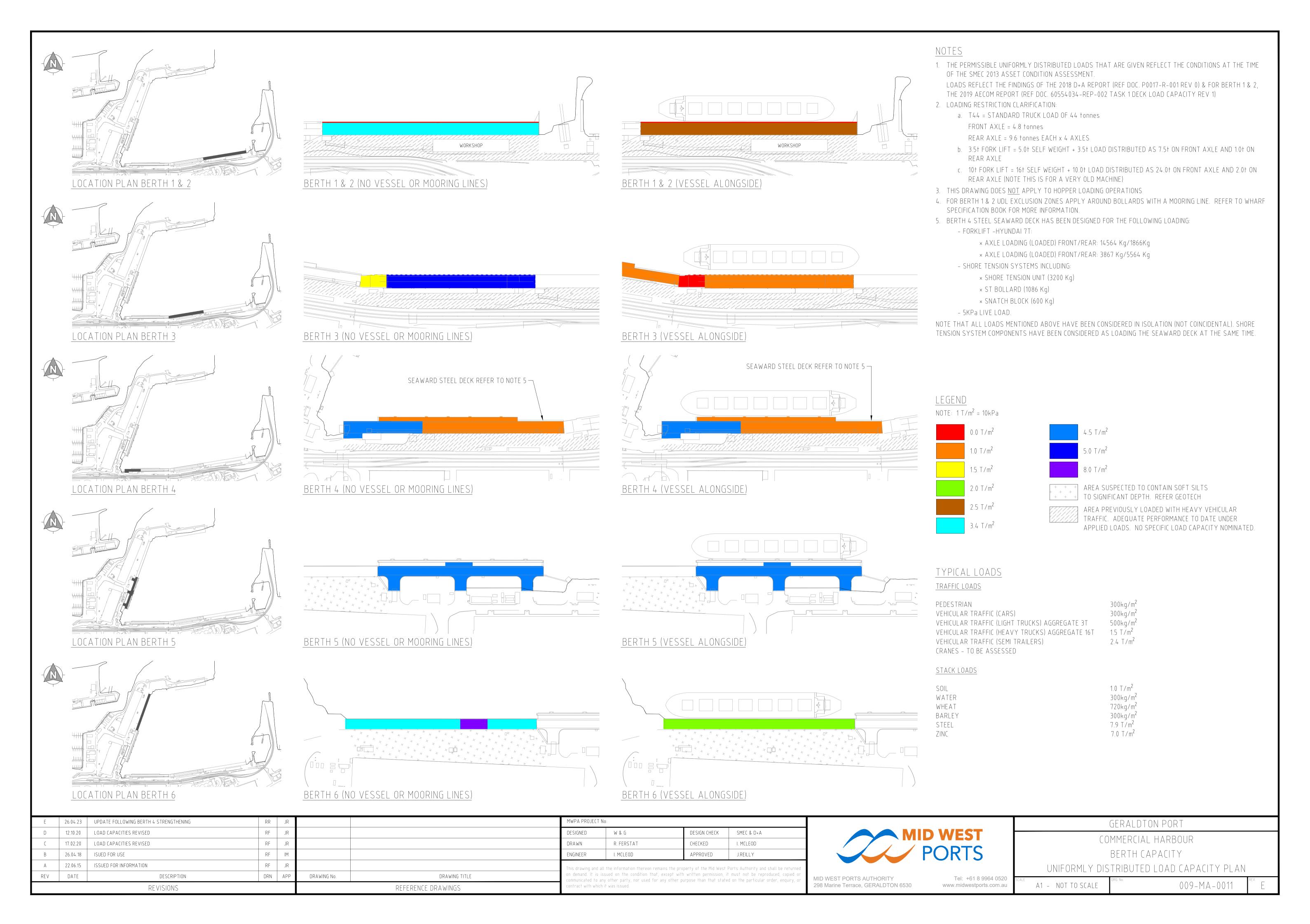


Appendix A

GERALDTON PORT – GENERAL ARRANGEMENT AND UDL CAPACITY PLAN

Title	Drawing Number	Rev Number
Port Infrastructure Features, Services and Facilities	010-G-0022	В
Commercial Harbour	009-MA-0011	E
Berth Capacity		
Uniformly Distributed Load Capacity Plan		



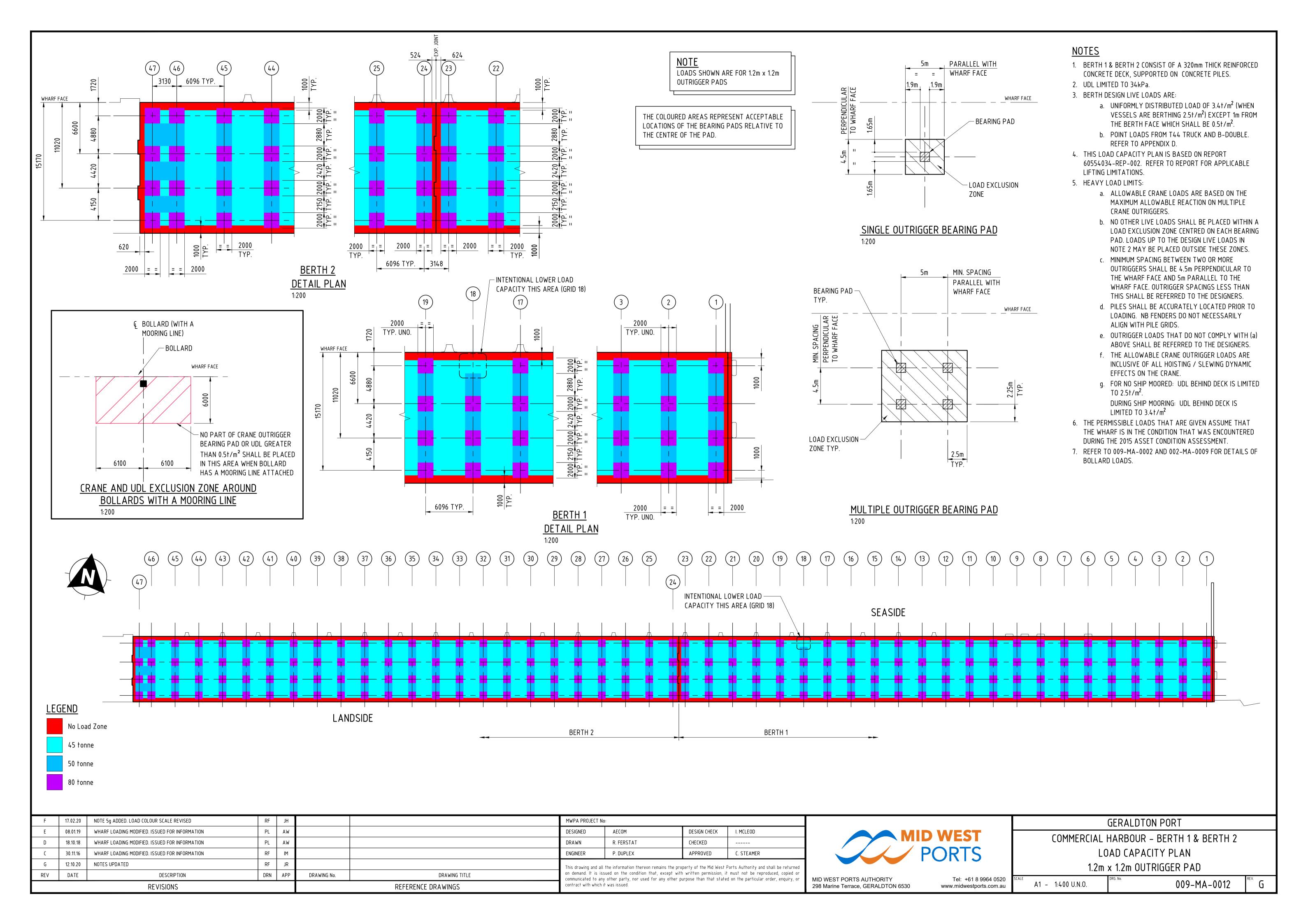


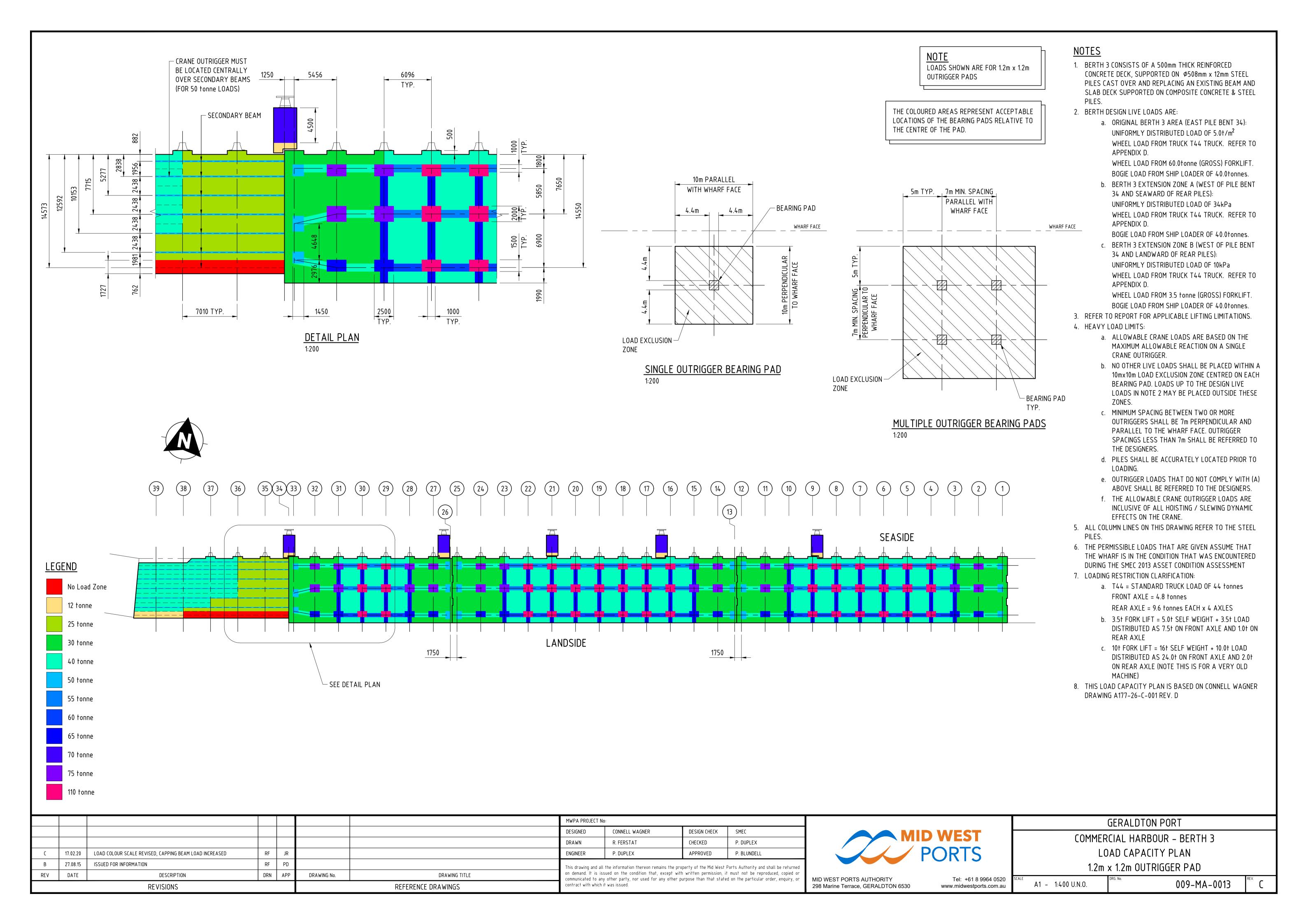


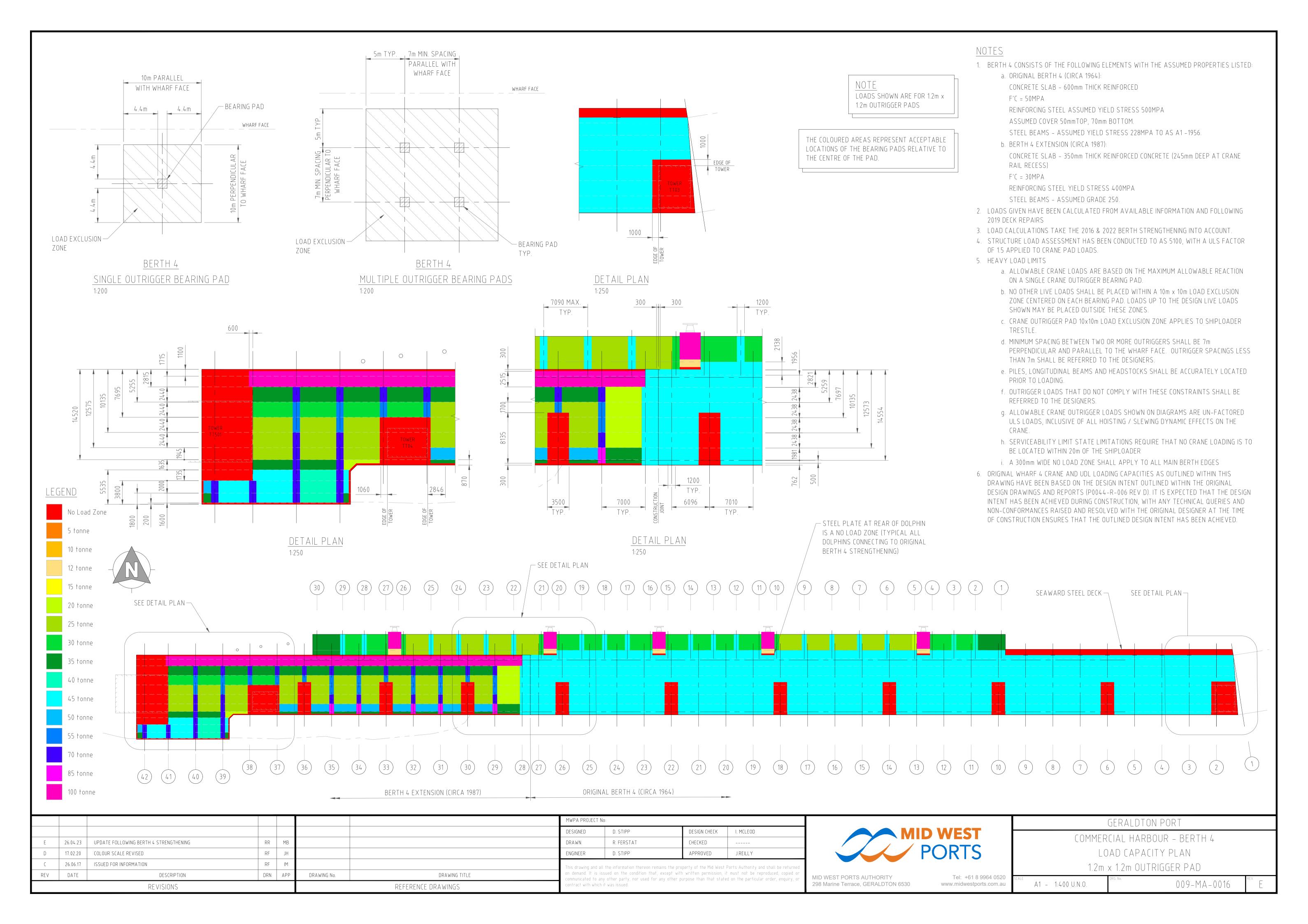
Appendix B

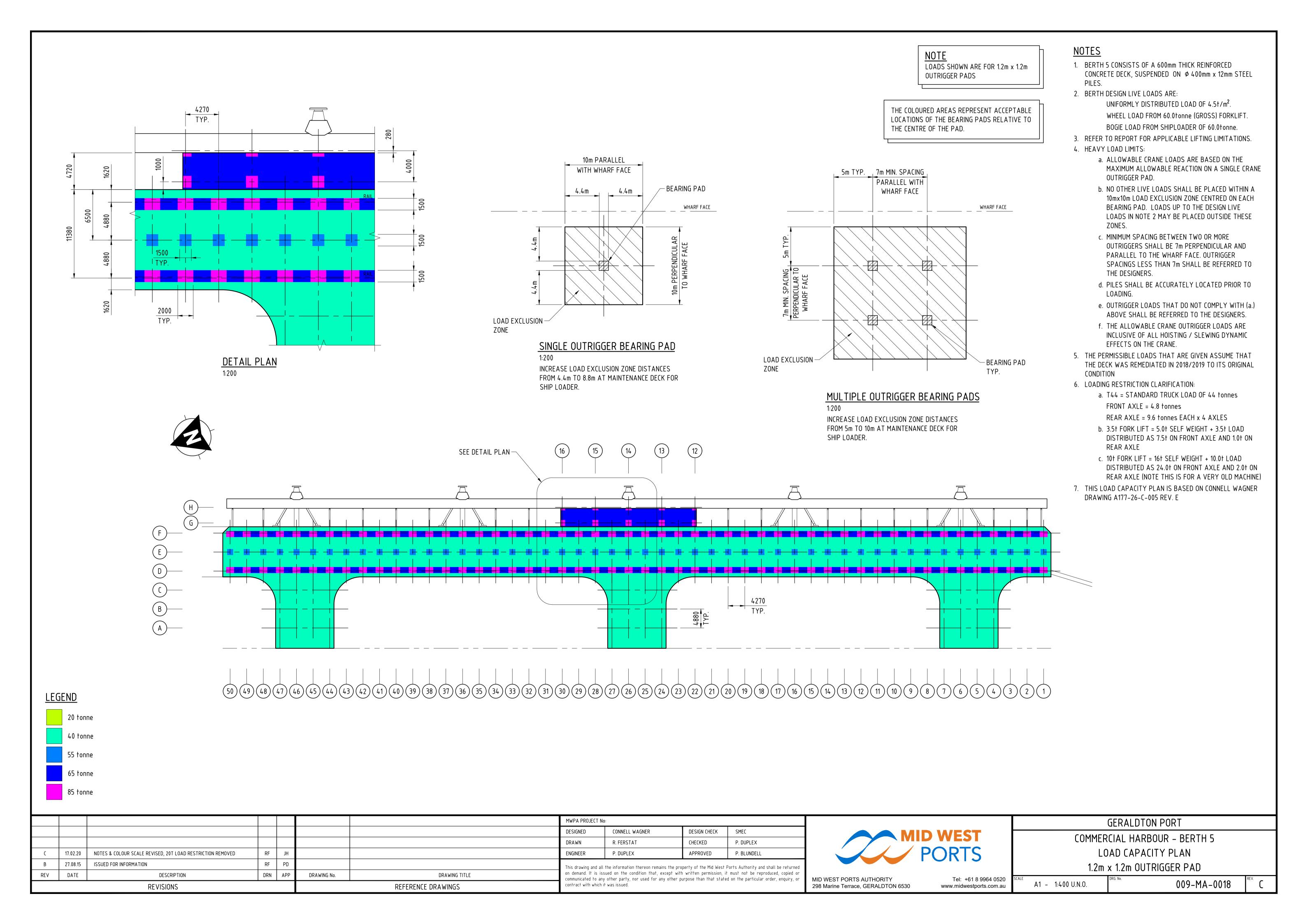
LOAD CAPACITY PLANS - 1.2M x 1.2M OUTRIGGERS AND CUSTOM ASSESSMENTS

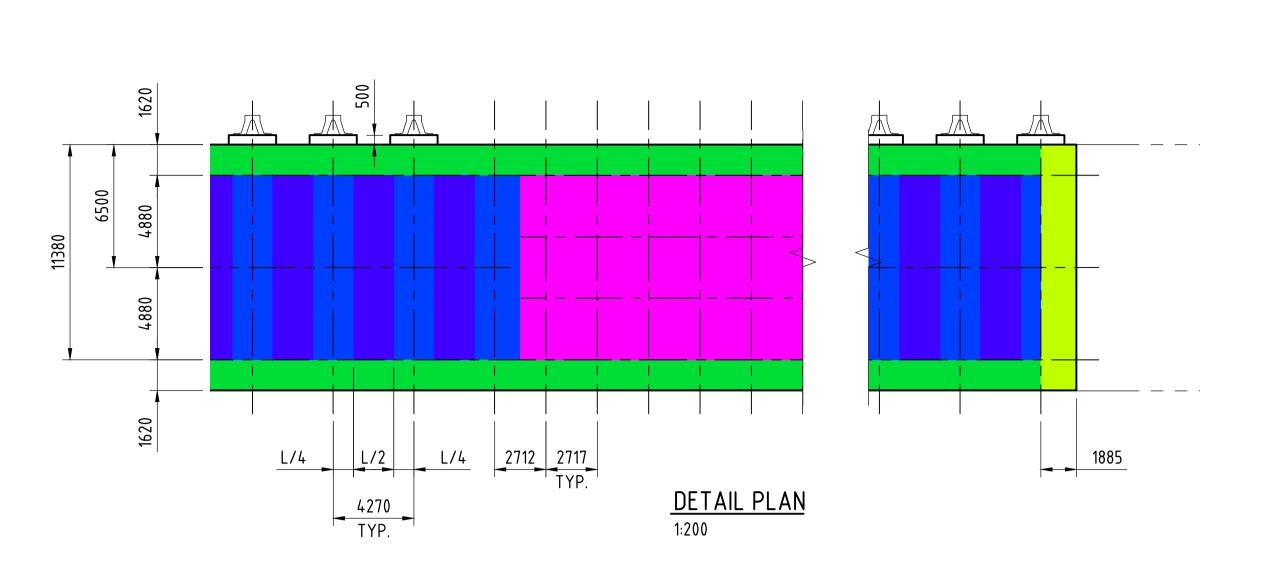
Berth Number	Title	Drawing Number	Rev Number
Berths 1 and 2	Commercial Harbour – Berth 1 and Berth 2 Load Capacity Plan 1.2m x 1.2m Outrigger Pad	009-MA-0012	G
Berth 3	Commercial Harbour – Berth 3 Load Capacity Plan 1.2m x 1.2m Outrigger Pad	009-MA-0013	С
Berth 4	Commercial Harbour – Berth 4 Load Capacity Plan 1.2m x 1.2m Outrigger Pad	009-MA-0016	D
Berth 5	Commercial Harbour – Berth 5 Load Capacity Plan 1.2m x 1.2m Outrigger Pad	009-MA-0018	С
Berth 6	Commercial Harbour – Berth 6 Load Capacity Plan 1.2m x 1.2m Outrigger Pad	009-MA-0020	С
Berth 6	Commercial Harbour – Berth 6 Stevens Hopper Arrangement Plan and Details	009-MA-0061	0
Berth 6 QUBE Liebherr LHM280 Crane	EX-B-1.01 EX-B-1.02	4 4 3	
		EX-B-1.03 EX-B-1.04	3











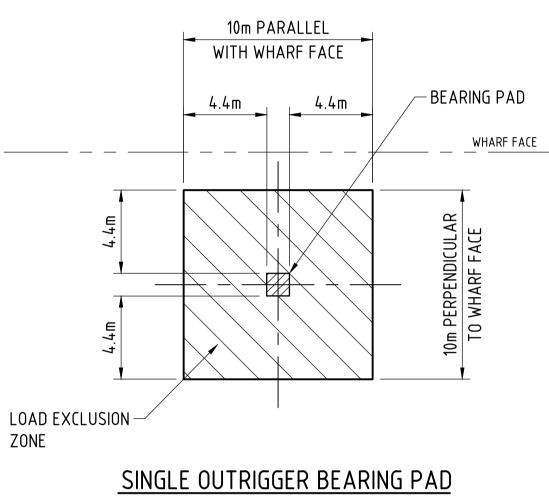
NOTE

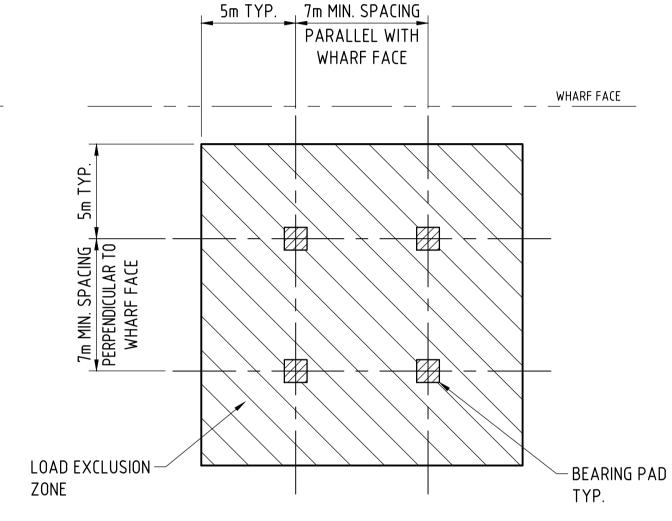
LOADS SHOWN ARE FOR 1.2m x 1.2m OUTRIGGER PADS

THE COLOURED AREAS REPRESENT ACCEPTABLE LOCATIONS OF THE BEARING PADS RELATIVE TO THE CENTRE OF THE PAD.

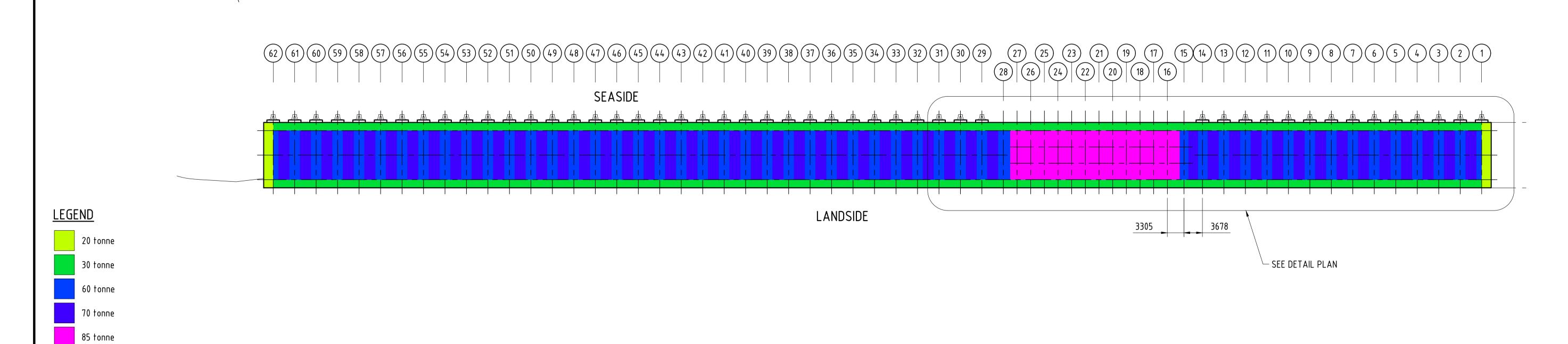
NOTES

- BERTH 6 CONSISTS OF A 300mm THICK REINFORCED CONCRETE DECK, SUSPENDED ON STEEL BEAMS, SUPPORTED ON Ø 406mm STEEL PILES.
- 2. BERTH DESIGN LIVE LOADS ARE:
 - a. LOAD OUT BRIDGE:
 - UNIFORMLY DISTRIBUTED LOAD OF 8.0+/m²
 - b. ELSEWHERE:
 - UNIFORMLY DISTRIBUTED LOAD OF 3.4†/m².
- 3. REFER TO REPORT FOR APPLICABLE LIFTING LIMITATIONS.
- 4. HEAVY LOAD LIMITS:
 - a. ALLOWABLE CRANE LOADS ARE BASED ON THE MAXIMUM ALLOWABLE REACTION ON A SINGLE CRANE OUTRIGGER PAD.
 - b. NO OTHER LIVE LOADS SHALL BE PLACED WITHIN A 10mx10m LOAD EXCLUSION ZONE CENTRED ON EACH BEARING PAD. LOADS UP TO THE DESIGN LIVE LOADS IN NOTE 2 MAY BE PLACED OUTSIDE THESE ZONES
 - c. MINIMUM SPACING BETWEEN TWO OR MORE OUTRIGGERS SHALL BE 7m PERPENDICULAR AND PARALLEL TO THE WHARF FACE. OUTRIGGER SPACINGS LESS THAN 7m SHALL BE REFERRED TO THE DESIGNERS.
 - d. PILES SHALL BE ACCURATELY LOCATED PRIOR TO LOADING.
 - e. OUTRIGGER LOADS THAT DO NOT COMPLY WITH (a.) ABOVE SHALL BE REFERRED TO THE DESIGNERS.
 - f. THE ALLOWABLE CRANE OUTRIGGER LOADS ARE INCLUSIVE OF ALL HOISTING / SLEWING DYNAMIC EFFECTS ON THE CRANE.
- 5. THE PERMISSIBLE LOADS THAT ARE GIVEN ASSUME THAT THE WHARF IS IN THE CONDITION THAT WAS ENCOUNTERED DURING THE SMEC 2013 ASSET CONDITION ASSESSMENT
- 6. THIS LOAD CAPACITY PLAN IS BASED ON CONNELL WAGNER DRAWING A177-26-C-007 REV. D





MULTIPLE OUTRIGGER BEARING PADS



contract with which it was issued.

							MWPA PROJECT No:			
							DESIGNED	CONNELL WAGNER	DESIGN CHECK	SMEC
							DRAWN	R. FERSTAT	CHECKED	P. DUPLEX
С	17.02.20	COLOUR SCALE REVISED	RF	JH			ENGINEER	P. DUPLEX	APPROVED	P. BLUNDELL
В	27.08.15	ISSUED FOR INFORMATION	RF	PD			This drawing and all	the information thereon remains the pro	operty of the Mid West I	Ports Authority and shall be returne
REV	DATE	DESCRIPTION	DRN	APP	DRAWING No.	DRAWING TITLE	on demand. It is iss	sued on the condition that, except wit	h written permission, it	t must not be reproduced, copied o

REVISIONS

REFERENCE DRAWINGS



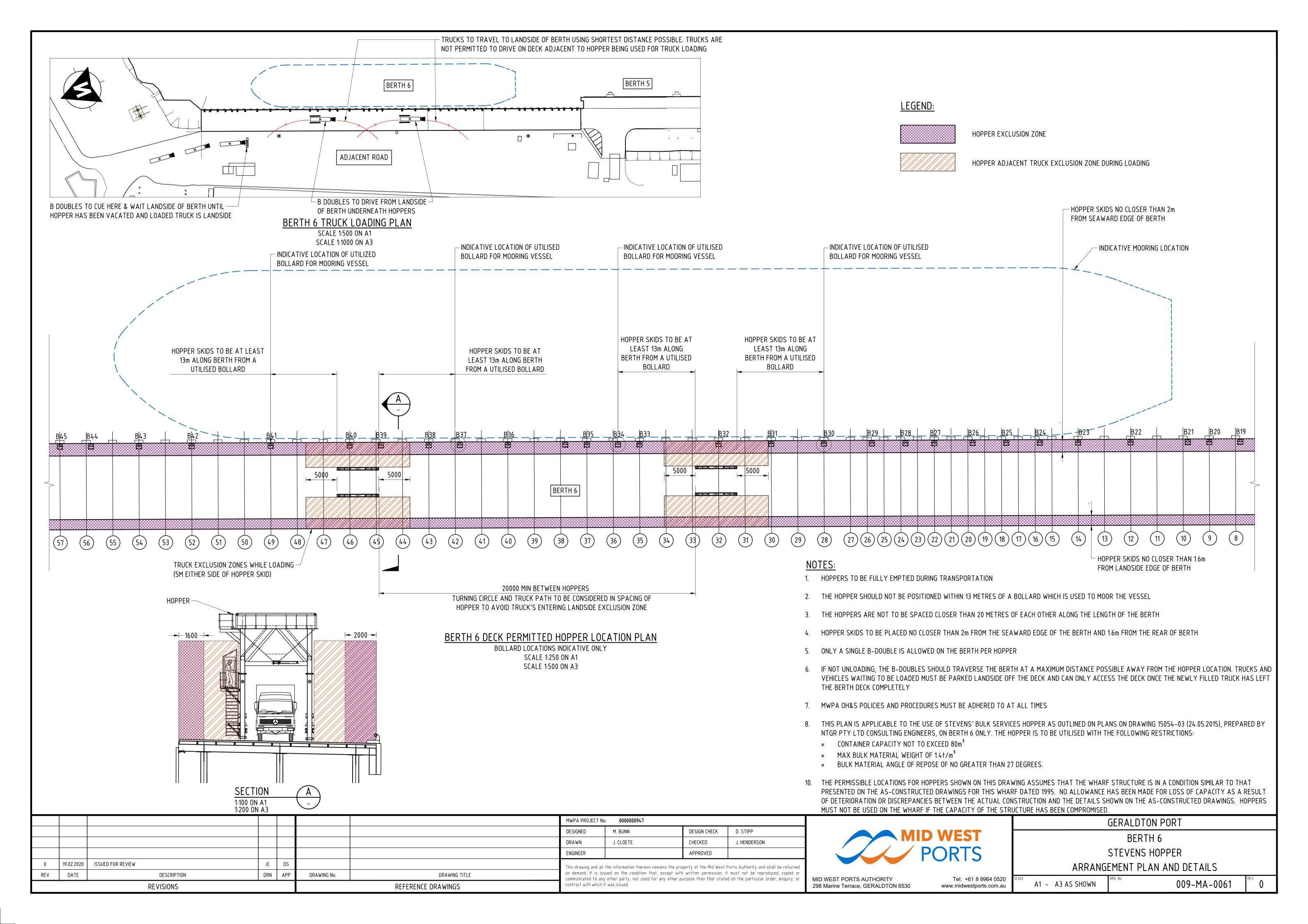
MID WEST PORTS AUTHORITY

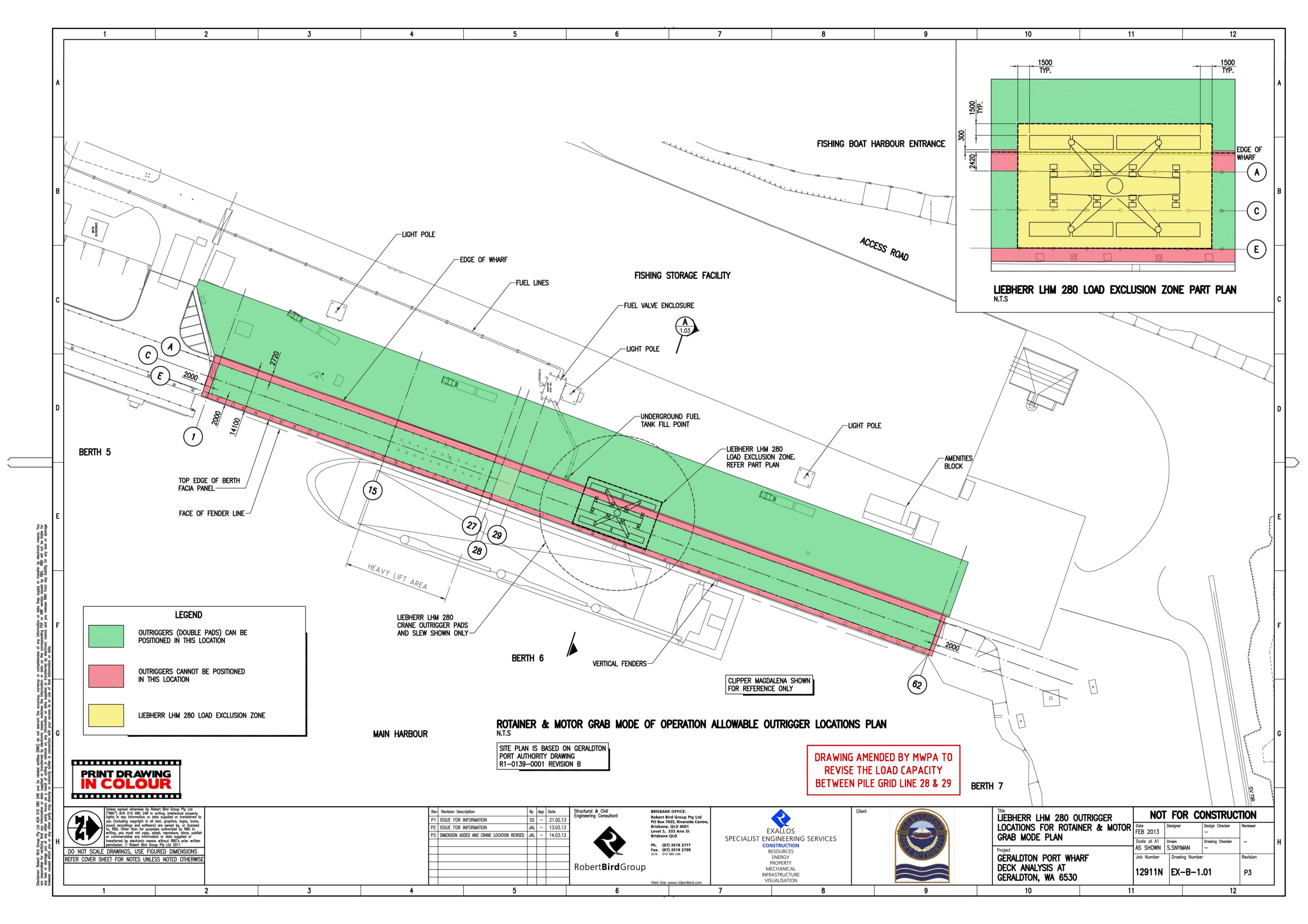
298 Marine Terrace, GERALDTON 6530

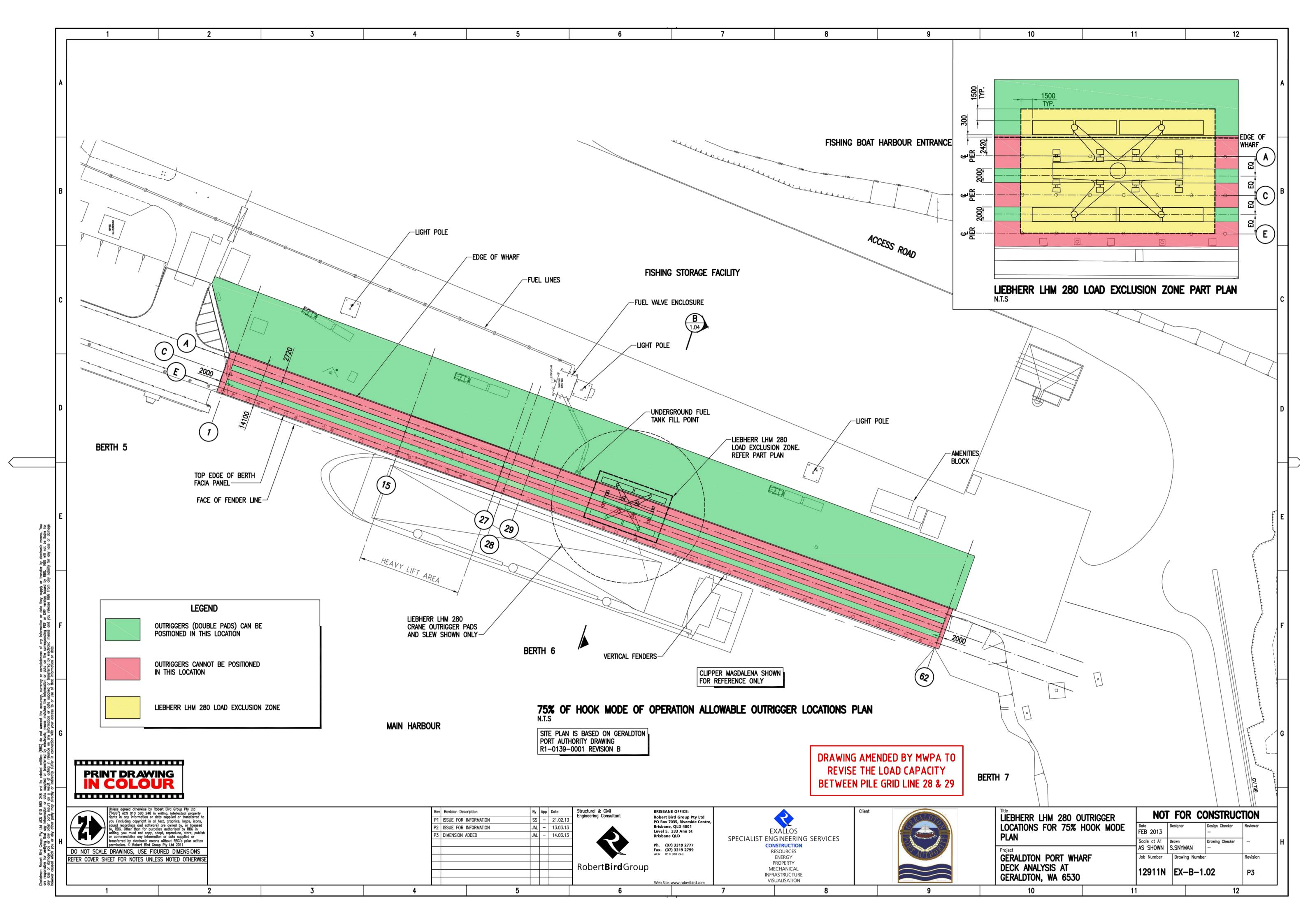
COMMERCIAL HARBOUR – BERTH 6 LOAD CAPACITY PLAN 1.2m x 1.2m OUTRIGGER PAD

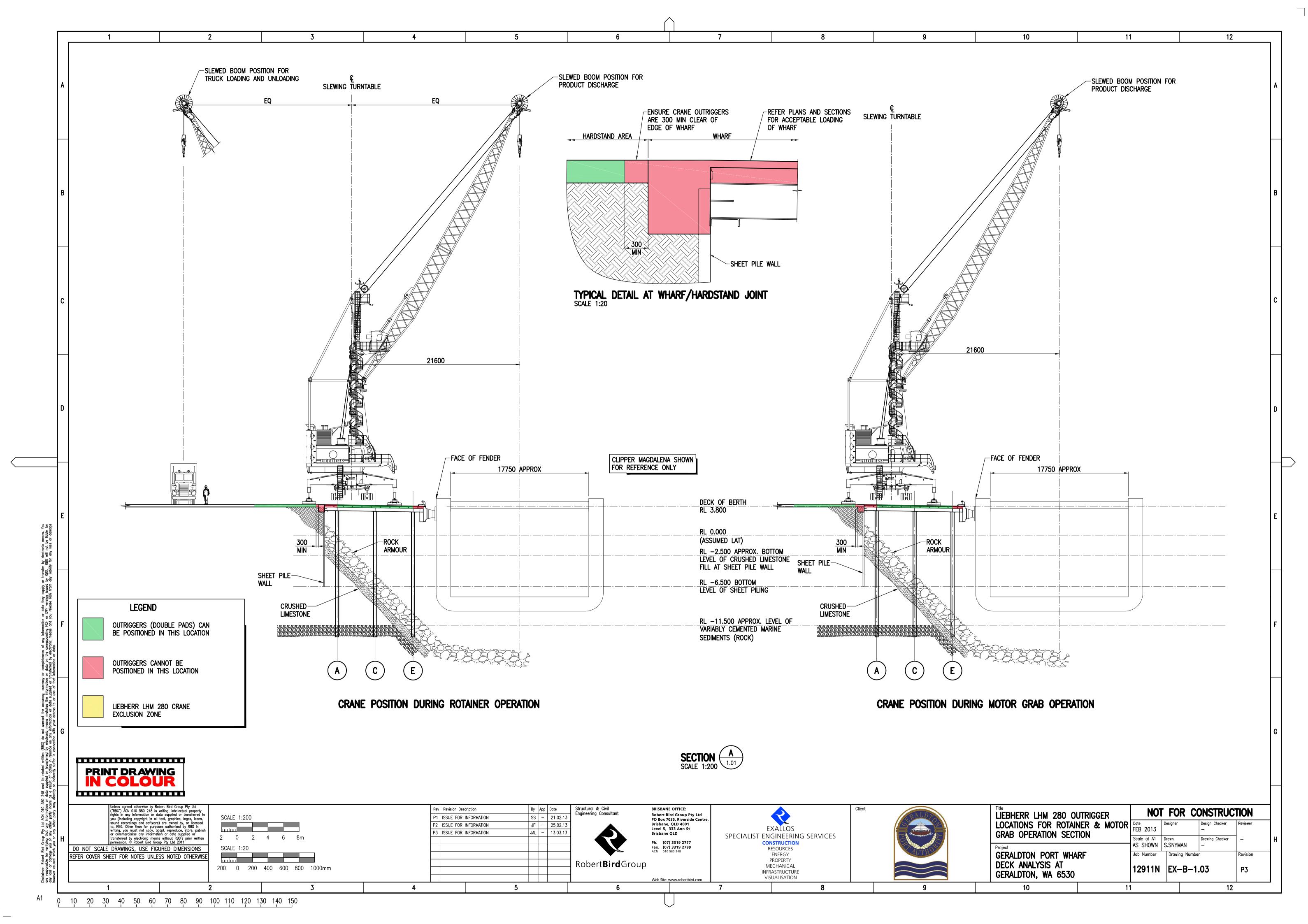
GERALDTON PORT

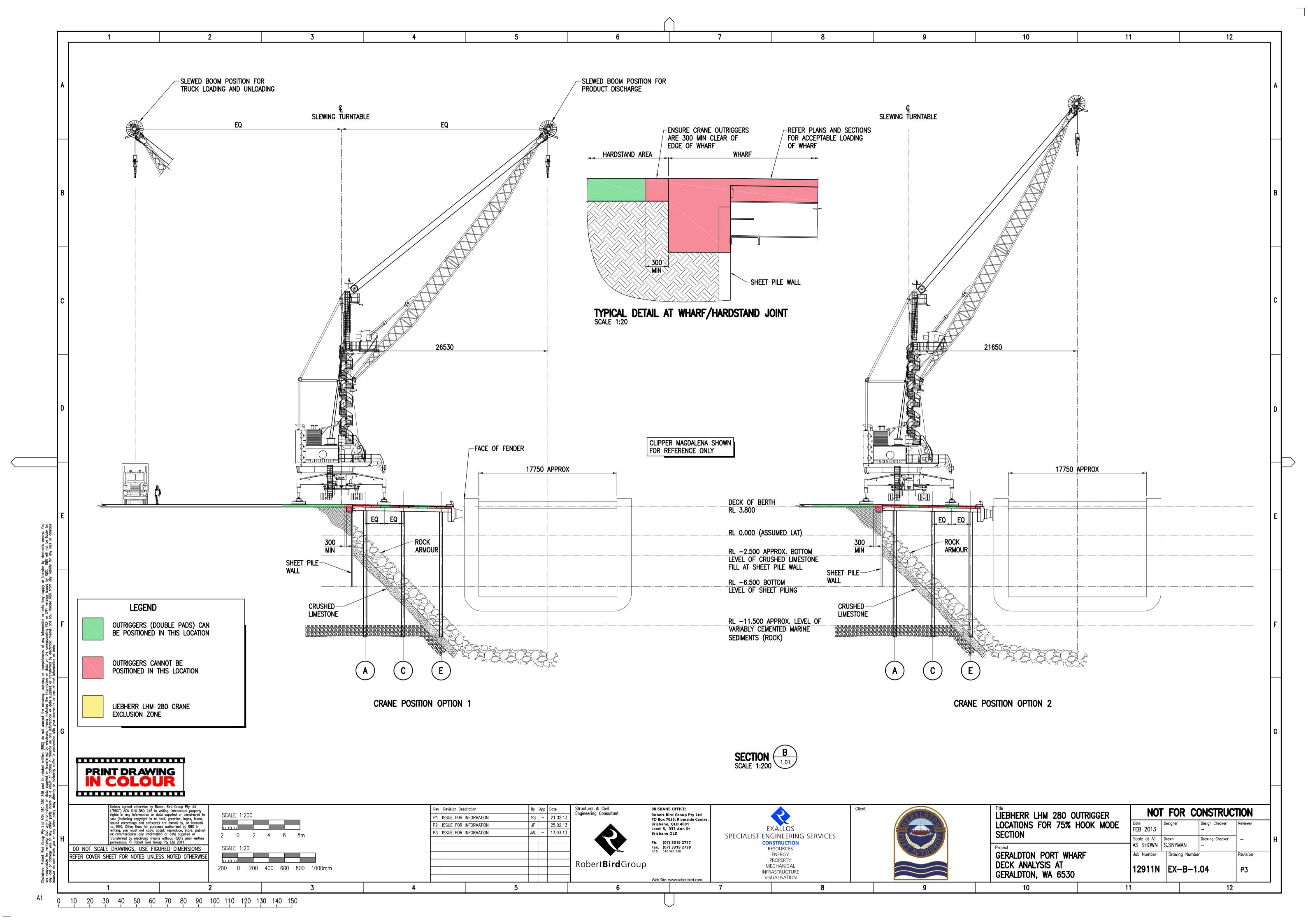
Tel: +61 8 9964 0520 www.midwestports.com.au SCALE A1 - 1:400 U.N.O.









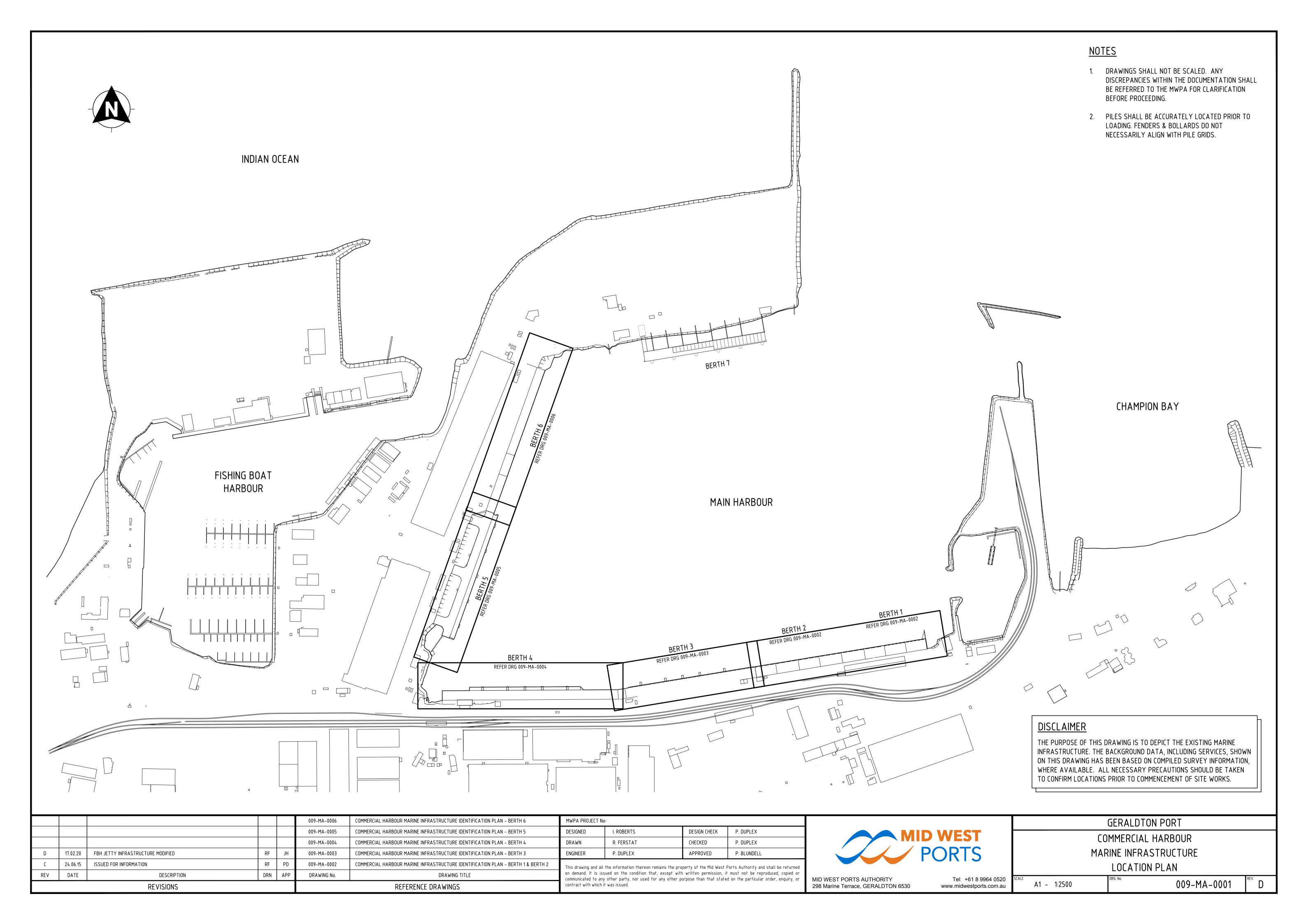


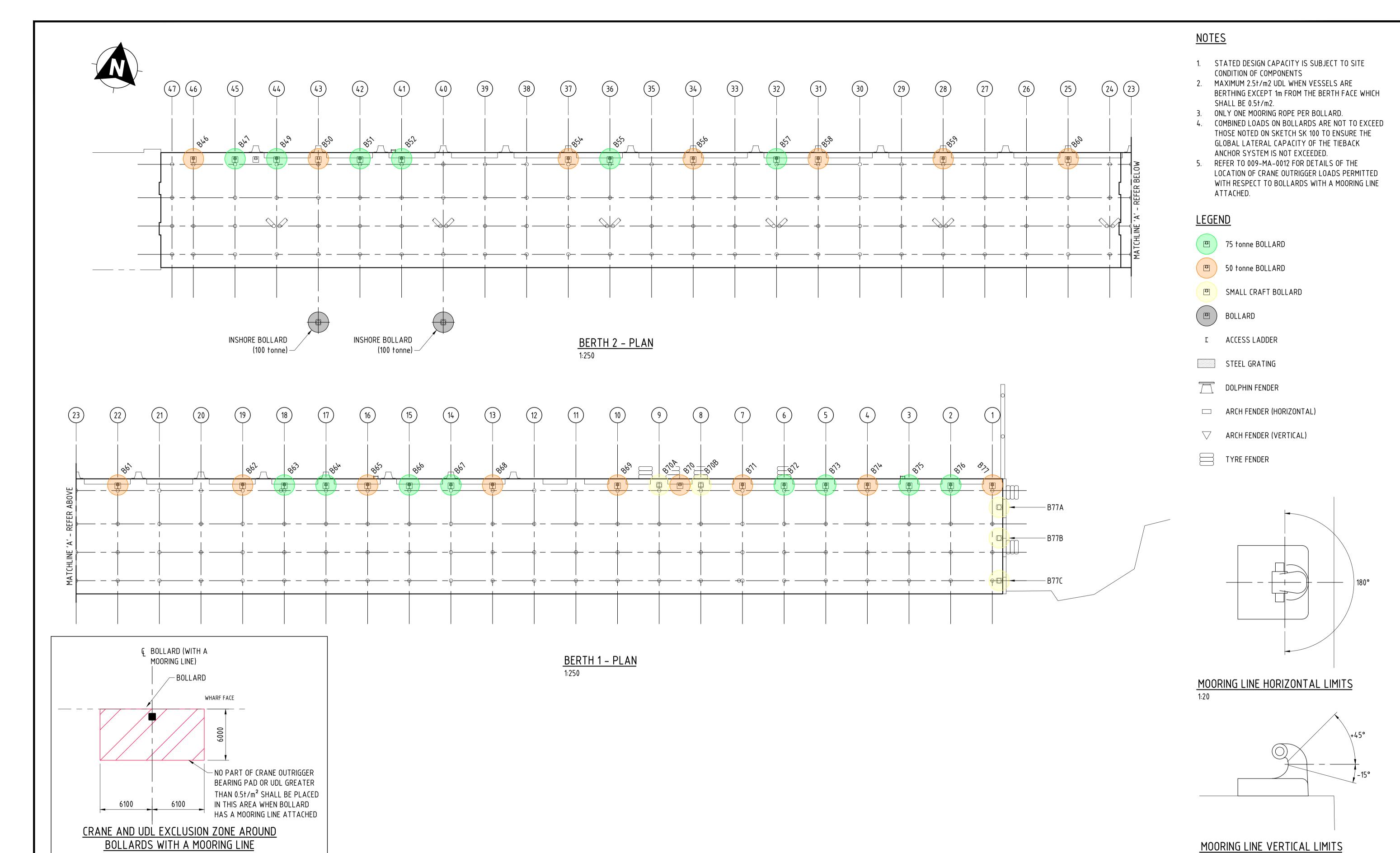


Appendix C

BOLLARD IDENTIFICATION AND CAPACITY PLANS

Title	Drawing Number	Rev Number
Commercial Harbour Marine Infrastructure Location Plan	009-MA-0001	D
Commercial Harbour Marine Infrastructure	009-MA-0002	J
Identification Plan – Berth 1 and Berth 2		
Berths 1 and 2 Maximum Combined Bollard Loads	002-MA-0009	А
Commercial Harbour Marine Infrastructure Identification Plan – Berth 3	009-MA-0003	G
Commercial Harbour Marine Infrastructure Identification Plan – Berth 4	009-MA-0004	F
Commercial Harbour Marine Infrastructure	009-MA-0005	Е
Identification Plan – Berth 5		
Commercial Harbour	009-MA-0006	M
Marine Infrastructure Identification Plan – Berth 6		





MWPA PROJECT No:

contract with which it was issued.

I. ROBERTS

R. FERSTAT

P. DUPLEX

DESIGN CHECK

CHECKED

APPROVED

P. DUPLEX

P. DUPLEX

P. BLUNDELL

DESIGNED

DRAWN

ENGINEER

1:200

UDL NOTE REMOVED

BOLLARD CAPACITIES REVISED

BOLLARD CAPACITIES REVISED

INSHORE BOLLARD CAPACITIES ADDED

BOLLARD 50 CAPACITY CHANGED AND UDL REVISED

DESCRIPTION

REVISIONS

009-MA-0001

DRAWING No.

DRN APP

COMMERCIAL HARBOUR MARINE INFRASTRUCTURE LOCATION PLAN

REFERENCE DRAWINGS

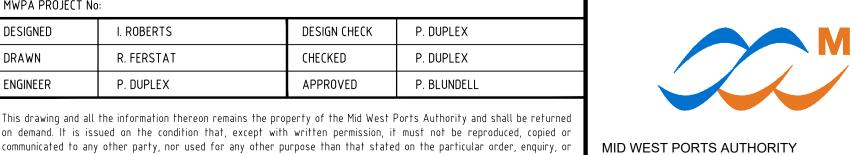
DRAWING TITLE

30.09.20

17.02.20

DATE

REV



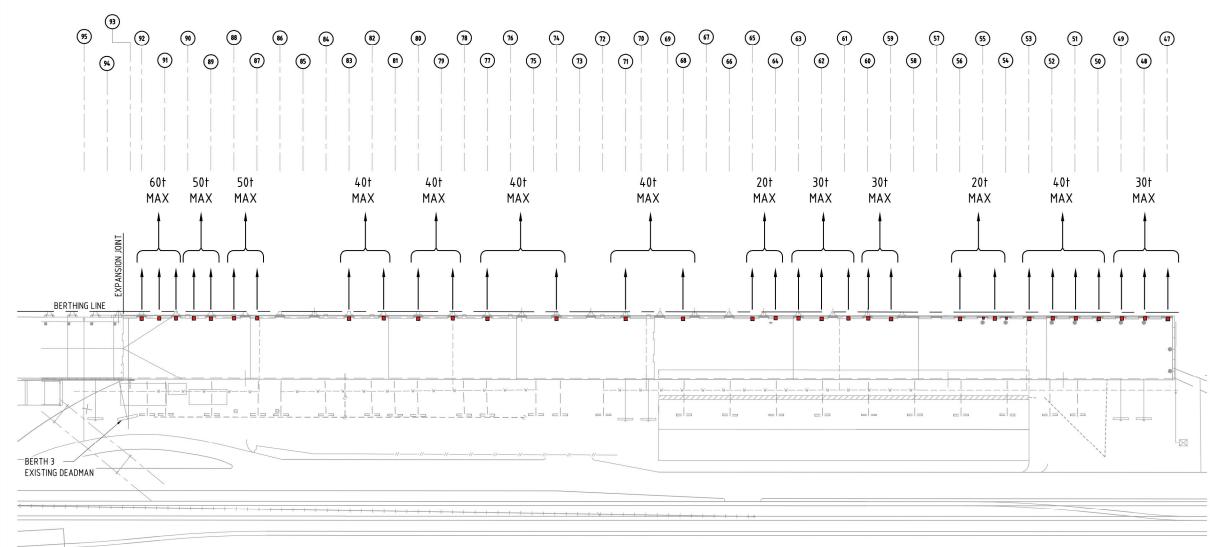
298 Marine Terrace, GERALDTON 6530

Tel: +61 8 9964 0520 A1 - 1:250 www.midwestports.com.au

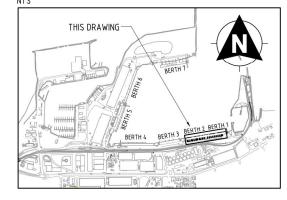
GERALDTON PORT COMMERCIAL HARBOUR MARINE INFRASTRUCTURE

IDENTIFICATION PLAN – BERTH 1 & BERTH 2





KEYPLAN NTS



GENERAL NOTES:

- THESE DRAWINGS SHALL BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS AND SPECIFICATIONS AND WITH SUCH OTHER WRITTEN INSTRUCTIONS AS MAY BE USED DURING THE COURSE OF THE CONTRACT. ALL DISCREPANCIES SHALL BE REFERRED TO THE MWPA PROJECT SUPERVISOR FOR DECISION BEFORE PROCEEDING WITH THE WORK.
- 2. DIMENSIONS SHALL NOT BE OBTAINED BY SCALING THE DRAWINGS.

LEGEND:

 EXISTING BOLLARD LOCATIONS (AS PER HTD SURVEY 02118AS1-1-0 DATED 27.03.2018)

MOORING CONCURRENT BOLLARD LATERAL LOADS 1:500

NOTE:

THE BOLLARD LATERAL LOADS SHOWN ARE ASSUMED TO BE APPLIED TO THE 31 BOLLARDS CONCURRENTLY AT A HORIZONTAL ANGLE OF 90 DEGREES TO THE WHARF LONGITUDINAL AXIS AND AT A VERTICAL INCLINATION OF 0 DEGREES.

THE MAGNITUDE OF THE CONCURRENT BOLLARDS LATERAL LOADS HAS BEEN SELECTED SO AS NOT TO EXCEED THE GLOBAL LATERAL CAPACITY OF THE TIEBACK ANCHOR SYSTEM.

FOR INFORMATION ONLY.
NOT ISSUED FOR CONSTRUCTION

AECOM

							MWPA PROJECT No: 911			
							DESIGNED	P. LONGSTAFF	DESIGN CHECK	A.W. WRIGHT
							DRAWN	P. LONGSTAFF	CHECKED	S.CHAINE
							ENGINEER	A.WRIGHT	APPROVED	A. SARANDILY
Α	08.01.19	FOR INFORMATION	PL	AW			This drawing and all	the information thereon remains the pr	operty of the Mid West	Ports Authority and shall be returned
REV	DATE	DESCRIPTION	DRN	APP	DRAWING No.	DRAWING TITLE	on demand. It is is	sued on the condition that, except wit	h written permission, i	t must not be reproduced, copied or
		DEVICIONS				DEEDENCE DDAWINGS	communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or			



GERALDTON PORT

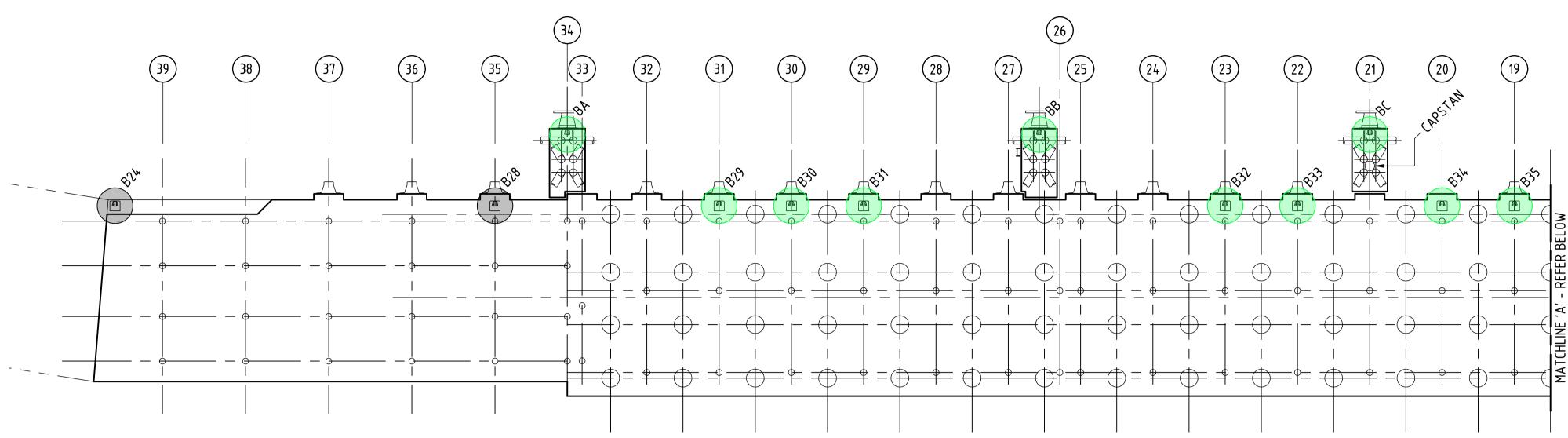
BERTH 1 & 2

MAXIMUM COMBINED

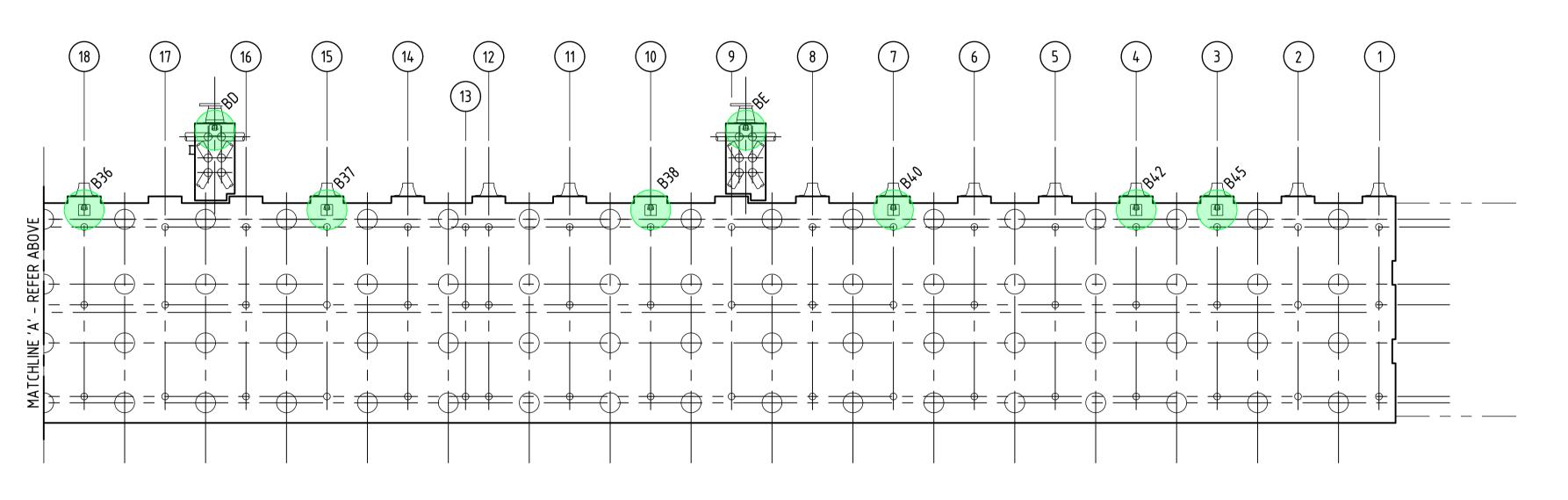
BOLLARD LOADS

A1 - 1:500 DRG. No.

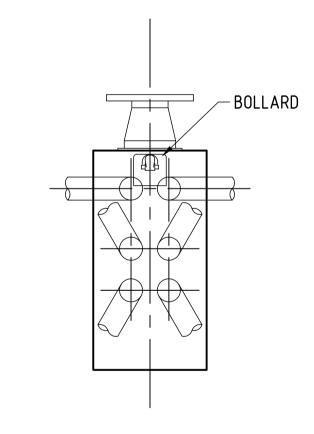




BERTH 3 - PART PLAN



BERTH 3 - PART PLAN



TYPICAL DOLPHIN PLAN

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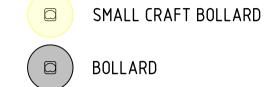
- 1. STATED DESIGN CAPACITY IS SUBJECT TO SITE CONDITION OF COMPONENTS
- 2. MAXIMUM 1t/m² UDL DURING MOORING

<u>LEGEND</u>

75 tonne BOLLARD



50 tonne BOLLARD





I ACCESS LADDER



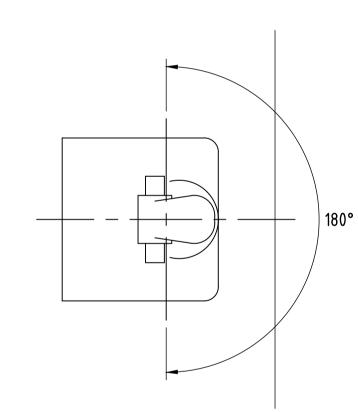




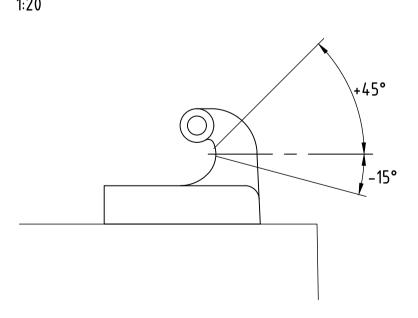








MOORING LINE HORIZONTAL LIMITS



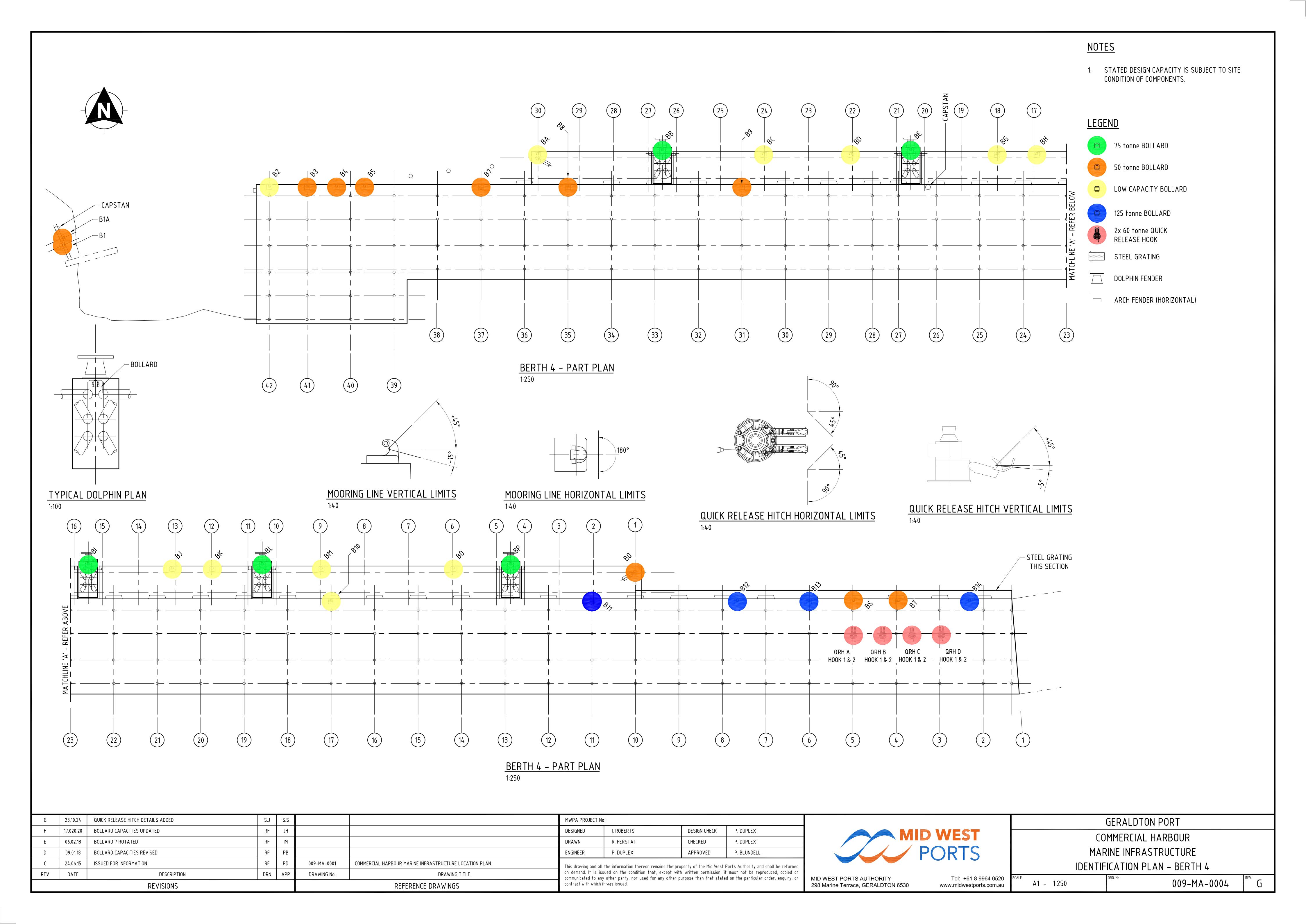
MOORING LINE VERTICAL LIMITS

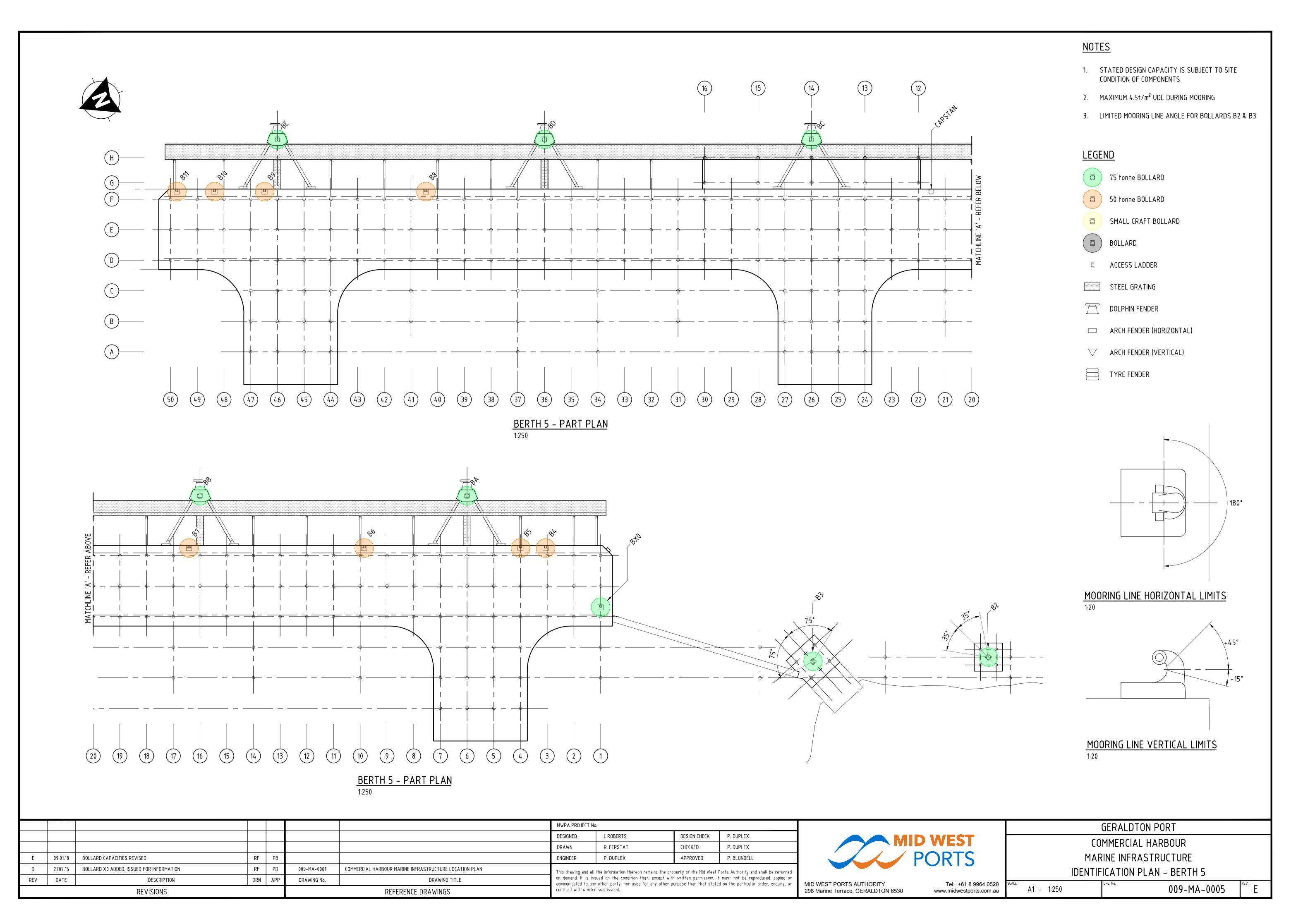
G	17.02.20	BOLLARD CAPACITIES UPDATED	RF	JH		MWPA PROJECT No	:		
F	30.04.18	BOLLARD 45 REMOVED	RF	IM		DESIGNED	I. ROBERTS	DESIGN CHECK	P. DUPLEX
E	06.02.18	BOLLARDS 25, 27, 39, 41 & 43 REMOVED	RF	IM		DRAWN	R. FERSTAT	CHECKED	P. DUPLEX
D	09.01.18	BOLLARD CAPACITIES REVISED	RF	РВ		ENGINEER	P. DUPLEX	APPROVED	P. BLUNDELL
С	24.06.15	ISSUED FOR INFORMATION	RF	PD	009-MA-0001 COMMERCIAL HARBOUR MARINE INFRASTRUCTURE LOCATION PLAN	This drawing and all	the information thereon remains the pro	perty of the Mid West F	Ports Authority and shall be returned
REV	DATE	DESCRIPTION	DRN	APP	DRAWING No. DRAWING TITLE	on demand. It is issued on the condition that, except with written permission, it must not be reproduced, copied or communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or			
	REVISIONS				REFERENCE DRAWINGS	contract with which it was issued.			

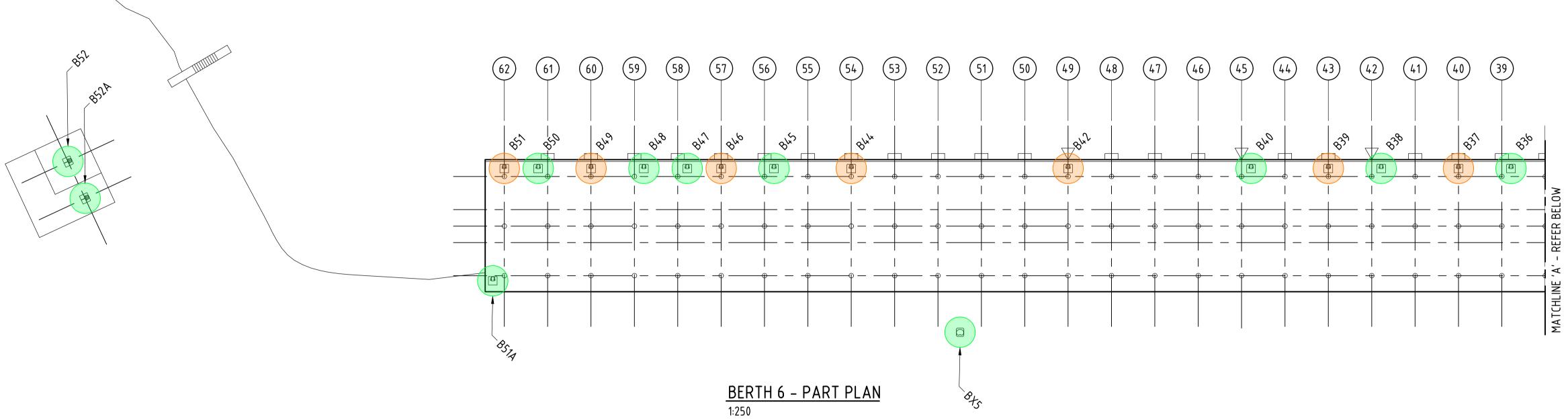


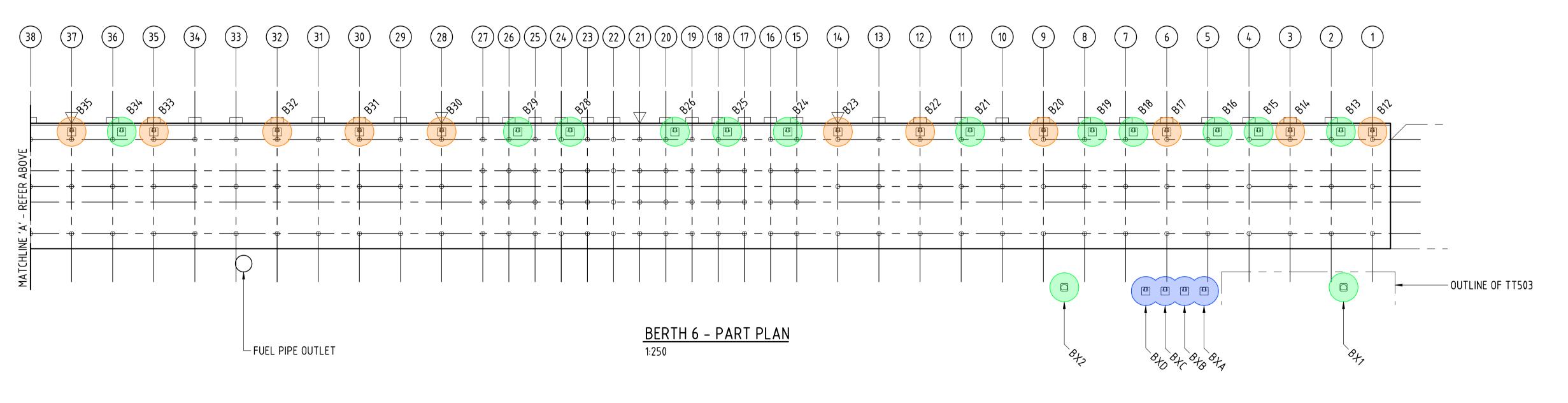
298 Marine Terrace, GERALDTON 6530

	GERALDTO	N PORT	
	COMMERCIAL	HARBOUR	
	MARINE INFRAS	STRUCTURE	
	IDENTIFICATION PL	AN – BERTH 3	
A1 - 1:250	DRG. No.	009-MA-0003	REV.









<u>NOTES</u>

- 1. STATED DESIGN CAPACITY IS SUBJECT TO SITE CONDITION OF COMPONENTS
- 2. MAXIMUM 2t/m² UDL DURING MOORING

<u>LEGEND</u>

125 tonne BOLLARD

75 tonne BOLLARD

50 tonne BOLLARD

SMALL CRAFT BOLLARD

BOLLARD

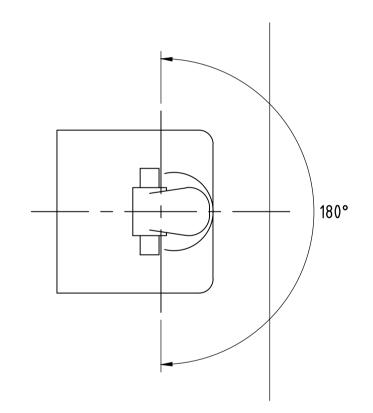
I ACCESS LADDER

STEEL GRATING

DOLPHIN FENDER

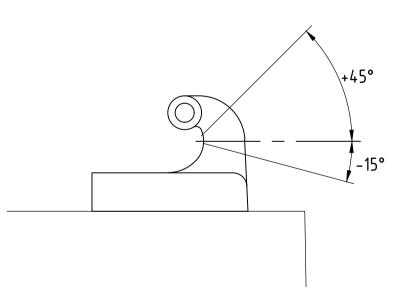
☐ ARCH FENDER (HORIZONTAL)

TYRE FENDER



MOORING LINE HORIZONTAL LIMITS

1:20



MOORING LINE VERTICAL LIMITS

Н	17.02.20	BOLLARD CAPACITIES REVISED	RF JH			MWPA PROJECT No:			
М	13.06.24	BOLLARD BXA, BXB, BXC, BXD, B51A ADDED	RF SS			DESIGNED	I. ROBERTS	DESIGN CHECK	P. DUPLEX
L	10.12.21	BOLLARDS RELOCATED	RF JH			DRAWN	R. FERSTAT	CHECKED	P. DUPLEX
K	30.09.20	BOLLARD CAPACITIES REVISED & LOCATIONS CORRECTED	RF JR			ENGINEER	P. DUPLEX	APPROVED	P. BLUNDELL
J	03.07.20	BOLLARD RATINGS REVISED FOLLOWING STRENGTHENING WORKS	RF GR	009-MA-0001	COMMERCIAL HARBOUR MARINE INFRASTRUCTURE LOCATION PLAN	This drawing and all the information thereon remains the property of the Mid West Ports Authority and shall be returned on demand. It is issued on the condition that, except with written permission, it must not be reproduced, copied or communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or			
REV	DATE	DESCRIPTION	DRN APP	DRAWING No.	DRAWING TITLE				
	REVISIONS				REFERENCE DRAWINGS	contract with which i			

MID WES	T
PORT	S

GERALDTON PORT	
COMMERCIAL HARBOUR	
MARINE INFRASTRUCTURE	
IDENTIFICATION PLAN – BERTH 6	

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0520 m.au A1 – 1:250

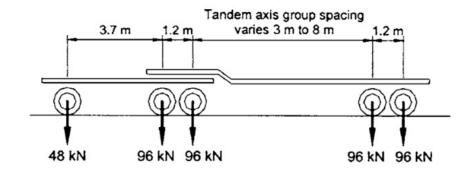
Appendix D

T44 AND B-DOUBLE TRUCK LOADING

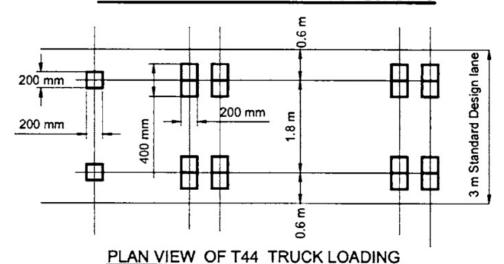
(T44 Extract from '92 Austroads Bridge Design Code)

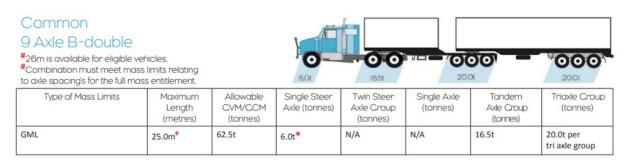
(B-Double from NHVR Website – National heavy vehicle mass and dimension limits July 2016)

(Current Freight Combinations from AS 5100.2 Supp 1 – 2007)



ELEVATION VIEW OF T44 TRUCK LOADING





Source: NHVR - National heavy vehicle mass and dimension limits



TABLE C6.2(C)

CURRENT LENGTH VEHICLES—CURRENT FREIGHT DENSITY = 0.28 t/m³

Vehicle	O/A length (m)	Gross mass (tonnes)	C	onfigurati	on, axle di (se	nd axle gr	oup mass	š	
Articulated	19.0	42.5	o 1.6 m 6 t	00 6.4 m 16.5 t	000 15.9 m 20 t				
B-double	25.0	62.5	o 1.6 m 6 t	00 5.6 m 16.5 t	000 13.6 m 20 t	000 22.6 m 20 t			
B-triple	33.0	82.5	o 1.6 m 6 t	oo 5.6 m 16.5 t	000 13.6 m 20 t	000 21.6 m 20 t	000 30.6 m 20 t		
RT triple	53.5	115.5	o 1.6 m 6 t	00 6.4 m 16.5 t	000 15.9 m 20 t	00 23.8 m 16.5 t	000 33.3 m 20 t	oo 41.2 m 16.5 t	000 50.7 m 20 t

NOTE: Distances are from front of vehicle to centre-line of axle group.



Appendix E

DYNAMIC LOAD FACTORS

(Extract from API Recommended Practice)

American Petroleum Institute

be designed for a horizontal force of 5% of the static sling load, applied simultaneously with the static sling load. This horizontal force should be applied perpendicular to the padeye at the center of the pinhole.

2.4.2.b. Static Loads. When suspended, the lift will occupy a position such that the center of gravity of the lift and the centroid of all upward acting forces on the lift are in static equilibrium. The position of the lift in this state of static equilibrium should be used to determine forces in the structure and in the slings. The movement of the lift as it is picked up and set down should be taken into account in determining critical combinations of vertical and horizontal forces at all points, including those to which lifting slings are attached.

2.4.2.c. Dynamic Load Factors. For lifts where either the lifting derrick or the structure to be lifted is on a floating vessel, the selection of the design lifting forces should consider the impact from vessel motion. Load factors should be applied to the design forces as developed from considerations of 2.4.2a and 2.4.2b.

For lifts to be made at open, exposed sea (i.e., offshore locations), padeyes and other internal members (and both end connections) framing into the joint where the padeye is attached and transmitting lifting forces within the structure should be designed for a minimum load factor of 2.0 applied to the calculated static loads. All other structural members transmitting lifting forces should be designed using a mini- mum load factor of 1.35.

For other marine situations (i.e., loadout at sheltered locations), the selection of load factors should meet the expected local conditions but should not be less than a minimum of 1.5 and 1.15 for the two conditions previously listed.

For typical fabrication yard operations where both the lifting derrick and the structure or components to be lifted are land-based, dynamic load factors are not required. For special procedures where unusual dynamic loads are possible, appropriate load factors may be considered.

2.4.2.d. Allowable Stresses. The lift should be designed so that all structural steel members are proportioned for basic allowable stresses as specified in Section 3.1. The AISC increase in allowable stresses for short-term loads should not be used. In addition, all critical structural connections and primary members should be designed to have adequate reserve strength to ensure structural integrity during lifting.

2.4.2.e. Effect of Tolerances. Fabrication tolerances and sling length tolerances both contribute to the distribution of forces and stresses in the lift system which are different from that normally used for conventional design purposes. The load factors recommended in Section 2.4.2c are intended to apply to situations where fabrication tolerances do not exceed the requirements of Section 11.1.5, and where the variation in length of slings does not exceed plus or minus ¼ of 1% of nominal sling length, or 1½ inches.

The total variation from the longest to the shortest sling should not be greater than $\frac{1}{2}$ of 1% of the sling length or 3 inches. If either fabrication tolerance or sling length tolerance exceeds these limits, a detailed analysis taking into account these tolerances should be performed to determine the redistribution of forces on both slings and structural members. This same type analysis should also be performed in any instances where it is anticipated that unusual deflections of particularly stiff structural systems may also affect load distribution.

2.4.2.f. Slings, Shackles and Fittings. For normal offshore conditions, slings should be selected to have a factor of safety of 4 for the manufacturer's rated minimum
breaking strength of the cable compared to static sling
load. The static sling load should be the maximum load
on any individual sling, as calculated in 2.4.2a,
b, and e above, by taking into account all components of
loading and the equilibrium position of the lift. This
factor of safety should be increased when unusually
severe conditions are anticipated, and may be reduced
to a minimum of 3 for carefully controlled conditions.

Shackles and fittings should be selected so that the

Shackles and fittings should be selected so that the manufacturer's rated working load is equal to or greater than the static sling load, provided the manufacturer's specifications include a minimum factor of safety of 3 compared to the minimum breaking strength.

2.4.3. Loadout Forces.

2.4.3.a. Direct Lift. Lifting forces for a structure loaded out by direct lift onto the transportation barge should be evaluated only if the lifting arrangement differs from that to be used in the installation, since lifting in open water will impose more severe conditions.

2.4.3.b. Horizontal Movement Onto Barge. Structures skidded onto transportation barges are subject to load conditions resulting from movement of the barge due to tidal fluctuations, nearby marine traffic and/or change in draft; and also from load conditions imposed by location, slope and/or settlement of supports at all stages of the skidding operation. Since movement is normally slow, impact need not be considered.

2.4.4. Transportation Forces

2.4.4.a. General. Transportation forces acting on templates, towers, guyed towers, minimum structures and platform deck components should be considered in their design, whether transported on barges or self-floating. These forces result from the way in which the structure is supported, either by barge or buoyancy, and from the response of the tow to environmental conditions encountered enroute to the site. In the subsequent paragraphs, the structure and supporting barge and the self-floating tower are referred to as the tow.

2.4.4.b. Environmental Criteria. The selection of environmental conditions to be used in determining the motions of the tow and the resulting gravitational and inertial forces acting on the tow should consider the following:

1. Previous experience along the tow route.

Extract from API Recommended Practice 2A – WSD(RP 2A-WSD) Twentieth Edition, July 1, 1993



Appendix F

DATUM DEFINITION DRAWING

			OLD PWD TIDAL BENCH MARK SET IN ORIGINAL DECK OF BERTH 1 (2.664m A.H.D.)
3.511m			
		 H.A.T. 1.2m	
		 M.H.H.W. 0.9m M.L.H.W. 0.8m	
	A	 M.S.L. 0.6m	AUSTRALIAN HEIGHT DATUM (A.H.D.) STATE MEAN SEA LEVEL
0.547m	0.847m	M.H.L.W. 0.3m M.L.L.W. 0.2m	
=		 L.A.T. 0.0m	NEW RAN CHART DATUM 2005 (NRCD)
0.3m			GERALDTON PORT DATUM AFTER 01-07-1956 TO 2004

MWPA PROJECT No:

contract with which it was issued.

D. MILLER

R. FERSTAT

P. DUPLEX

DESIGN CHECK

CHECKED

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on demand. It is issued on the condition that, except with written permission, it must not be reproduced, copied or

communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or

APPROVED

P. DUPLEX

P. DUPLEX

P. BLUNDELL

MID WEST PORTS AUTHORITY

298 Marine Terrace, GERALDTON 6530

DESIGNED

DRAWN

ENGINEER

DRAWING TITLE

REFERENCE DRAWINGS

24.06.15

DATE

REV

DATA TRANSFERRED FROM GPA DRAWING 010-MA-0004

DESCRIPTION

REVISIONS

DRN APP

DRAWING No.

<u>NOTES</u>

- ALL MARITIME CONSTRUCTION WILL BE CHART DATUM (NRCD)
- 2. ALL ONSHORE STRUCTURAL CONSTRUCTION WILL BE AUSTRALIAN HEIGHT DATUM (AHD.)
- KEY INTERFACE LEVELS ON DRAWING WILL USE BOTH NRCD & AHD DATUMS
- 4. HORIZONTAL DATUM CO-ORDINATES RELATE TO GCG94
- 5. THIS DRAWING IS BASED ON INFORMATION SUPPLIED BY DRAWING No. GPA05-DATUM-01-B (REV B)

<u>LEGEND</u>

L.A.T.

H.A.T.	HIGHEST ASTRONOMICAL TIDE
M.H.H.W.	MEAN HIGH HIGH WATER
M.L.H.W.	MEAN LOW HIGH WATER
M.S.L.	MEAN SEA LEVEL
M.H.L.W.	MEAN HIGH LOW WATER
M.L.L.W.	MEAN LOW LOW WATER

LOWEST ASTRONOMICAL TIDE

GERALDTON PORT
COMMERCIAL HARBOU

Tel: +61 8 9964 0520

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COMMERCIAL HARBOUR CHART DATUM DATUM SUMMARY – 2007

A1 - 1:20 DRG. No. 009-MA-0007

Table 2 from Aecom 60333556-REP-001 2014

Table 2 Berthing Capacity of Design Vessel for each Berth expressed as Maximum Approach Velocity for Normal and Abnormal conditions.

	1000	Approach C Balla		Approach Cap	acity Laden ²	Proposed Design
Berth	Vessel Size	Displacement (tonne)	Velocity (m/sec)	Displacement (tonne)	Velocity (m/sec)	Limit ³ (m/sec)
1	No fenders not examined					
2	Handymax Bulk, 50,000 DWT (LOA 190m, Beam 32.2m)	29,500	0.115	49,000	0.08/0.10	
	Large Handysize, 30,000 DWT (LOA 170m, Beam 25.3m)	20,000	0.12	32,000	0.09/0.11	0.18
	Small Handysize, 20,000 DWT (LOA 140m, Beam 25.0m)	14,000	0.14	26,000	0.10/0.12	
3/4/5	Panamax Bulk, 87,000 DWT (LOA 229m, Beam m)	49,000	0.14	68,000	0.12/0.14	
	Panamax Bulk, 70,000 DWT (LOA 225m, Beam 32.26m)	42,000	0.16	58,000	0.14/0.16	0.16
	Handysize Bulk, 30,000 DWT (LOA 170m, Beam 25.3m)	20,000	0.20	32,000	0.15/0.18	
6	Panamax Bulk, 70,000 DWT (LOA 225m, Beam 32.26m)	42,000	0.1	58,000	0.08/0.01	
	Handymax Bulk, 56,000 DWT (LOA 190m, Beam 32.26m)	33,000	0.10	51,000	0.08/0.10	
	Product Tanker, 26,500 DWT (LOA 160m, Beam 24.4m)	18,500	0.13	34,000	0.09/0.11	0.16
	Product Tanker (LOA189 m, Beam 32.2m)	Not applicable		67,000	0.07/0.09°	
	General Cargo, 18,500 DWT (LOA 157m, Beam m)	Not applicable		24,000	0.10/0.13	
7	Mini Cape, 115,000 DWT (LOA 254m, Beam 43m)	68,000	0.22	88,000	0.2/0.24	
	Post Panamax Bulk, 93,000 DWT (LOA 235m, Beam 38m)	54,000	0.24	72,000	0.22/0.24	0.17
	Panamax Bulk, 70,000 DWT (LOA 225m, Beam 32.26m)	42,000	0.27	58,000	0.22/0.25	

Normal Berthing Condition.

Legend

Meets PIANC and Proposed Design Limit
Meets PIANC, but not Proposed Design Limit
Considered a risk for berthing at anything other than very shallow angles

² Max Draft 10.0m, larger vessels are part laden. Velocity is Normal/Abnormal.

³ Suggested revision of PIANC criteria to suit Geraldton.

⁴ For bow impact in this case.

⁵ Indicates Value estimated from Approach velocity curves (refer section 6.4)



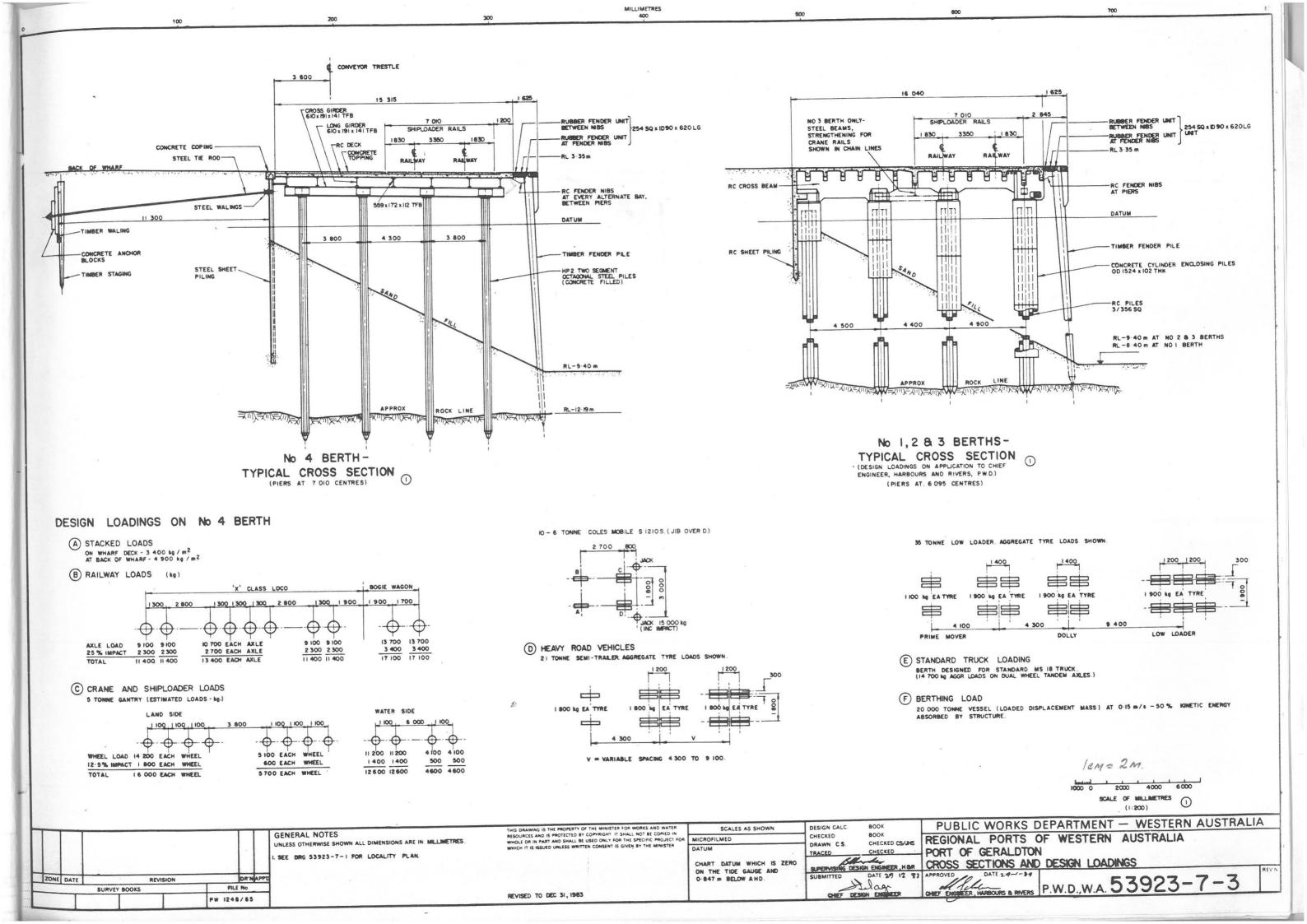
Appendix G

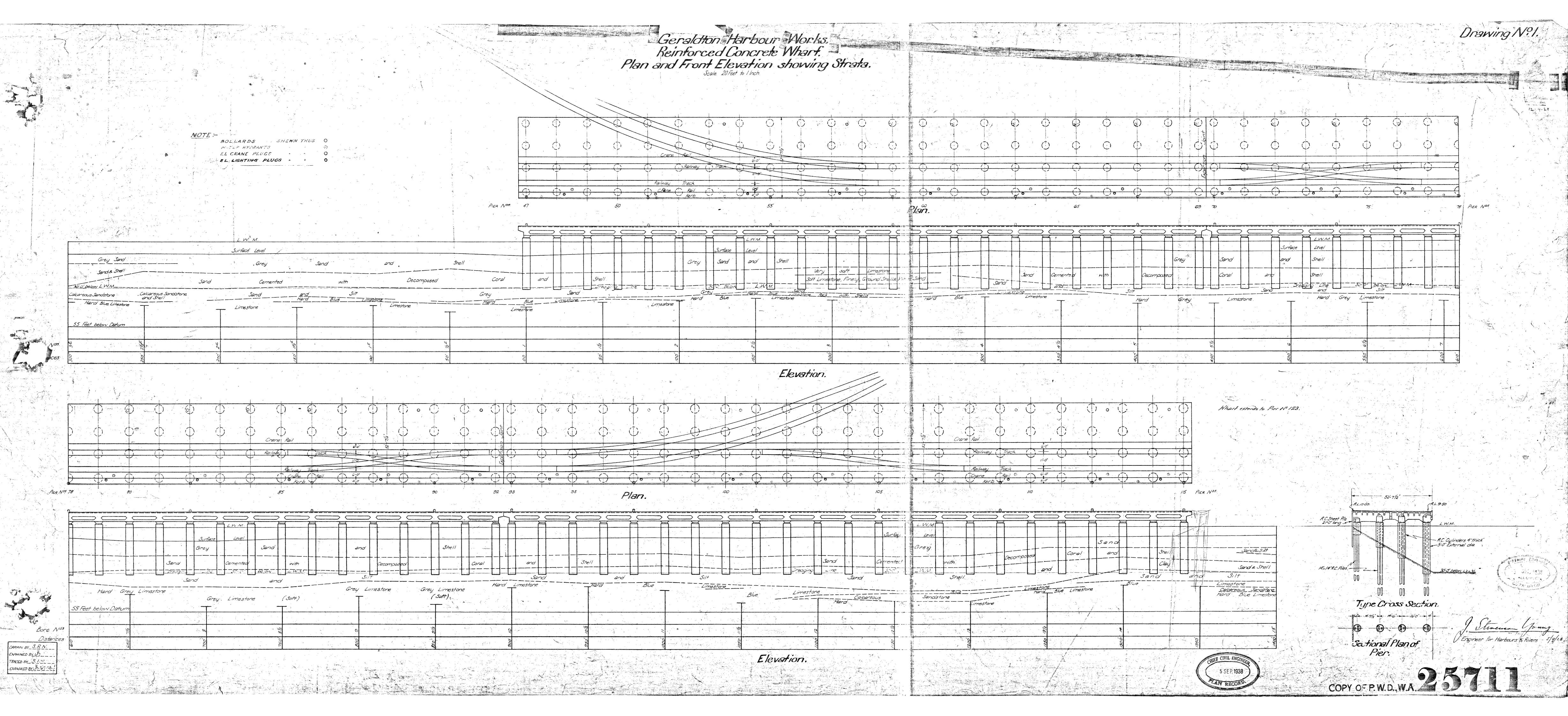
BERTH GENERAL ARRANGEMENTS AND SECTIONS

Title	Drawing Number	Rev Number
Berths 1, 2, 3 and 4		
Regional Ports of Western Australia, Port of Geraldton, Cross Sections and Design Loadings	53923-7-3	Circa 1983
Berths 1 and 2		
Original Berth 1, 2 + 3 Plan and Front Elevation	25711-1	Circa 1928
Typical Cross Section and Elevation of Wharf	25711-2	Circa 1928
Reinforced Concrete Piles	25711-3	Circa 1928
Original Berth 1, 2 + 3 Cross Beam	25711-14	Circa 1928
Rehabilitation of Berths 1 and 2, General Arrangement Cross-Sections	MP5566-002	3
Berth 1 and 2 Tieback Layout 1	002-C-0004	0
Berth 1 and 2 Tieback Layout 2	002-C-0005	0
Berth 1 and 2 Permanent Remediation Works Tie Rod Details	60554034-SK017	0
Berth 3		
No. 3 Berth Extension, General Cross Section	PWD	Circa 1961
Reconstruction of Berth No. 3, Existing Berth Cross Section	MP4102-03	1
Reconstruction of Berth No. 3, General Arrangement Section and	1404400 05	
Elevation of Fendering	MP4102-05	1
Geraldton Harbour Berth No. 3, General Arrangement	A177-26-C-002	С
Geraldton Port Enhancement Project, Modification to Berths 3 and 4	44045 LIDC DDE 354	2
Berth 3 — Section, Details and Dolphin Fixtures Setout	44915-URS-DPE-354	3
Berth 4	1	
No. 4 Berth, Details of Longitudinal Beams	PWD 39195	Circa 1961
No. 4 Berth Extensions, Deck Steelwork Plan	10765C/3D	D
Geraldton Harbour Berth No. 4, General Arrangement	A177-26-C-004	С
Modification to Berths 3 and 4, Berth 4 - Sections	44915-URS-DPE-358	3
Modification to Berths 3 and 4, Berth 4 Drainage	44915-URS-DPE-371	2
Typical Section Through Berth		
Berth 5	1	
Regional Ports of Western Australia, Port of Geraldton, Cross Sections	53923-7-4	Circa 1984
and Design Loadings		
Geraldton Harbour Berth No. 5, General Arrangement	A177-26-C-006	С
Berth 5, Design Criteria	75309405-3541	1
Berth 5, General Arrangement Sections – Sheet 1 of 3	75309405-3546	1
Berth 6	•	
Geraldton Harbour No. 6 Berth, Pile Layout and Sections	14228-S2	D
Geraldton Harbour No. 6 Berth, Sheet Piling Plan and Sections	14228-S3	D
Geraldton Harbour No. 6 Berth, Precast Concrete Panels and Steelwork	14228-S4	D
Plan Area 1		



Title	Drawing Number	Rev Number
Modification to Berth 6 Pile Retaining Wall, As Constructed Plan 2 of 4	44915-URS-DPE-439	В
Modification to Berth 6 Pile Retaining Wall, As Constructed Plan 3 of 4	44915-URS-DPE-440	В
Modification to Berth 6 Pile Retaining Wall, As Constructed Plan 4 of 4	44915-URS-DPE-441	В
Berth 6 Retaining Piles, Typical Section	44915-DPE-443	1

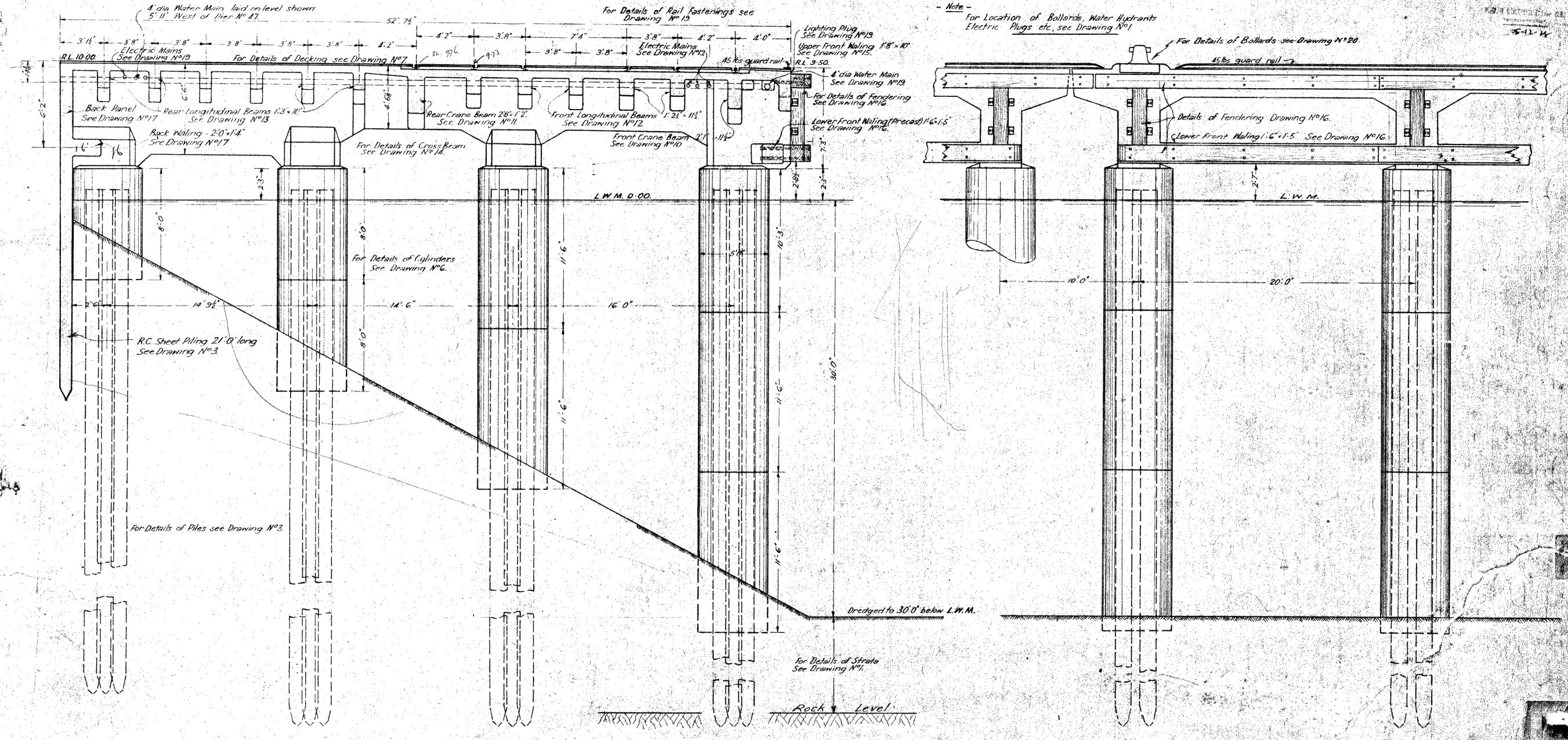




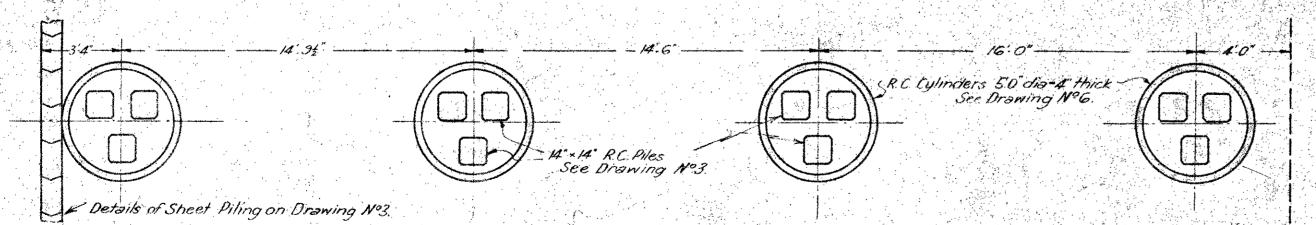
Geraldton Harbour Works. Reinforced Concrete Wharf. Type Cross Section and Elevation of Wharf.

-Scale - 4 Feet to I Inch.





Type Cross Section



Sectional Plan through Cylinders

Part Elevation

Geraldton Harbour Works. Reinforced Concrete Wharf. Type Cross Section and Elevation of Whar

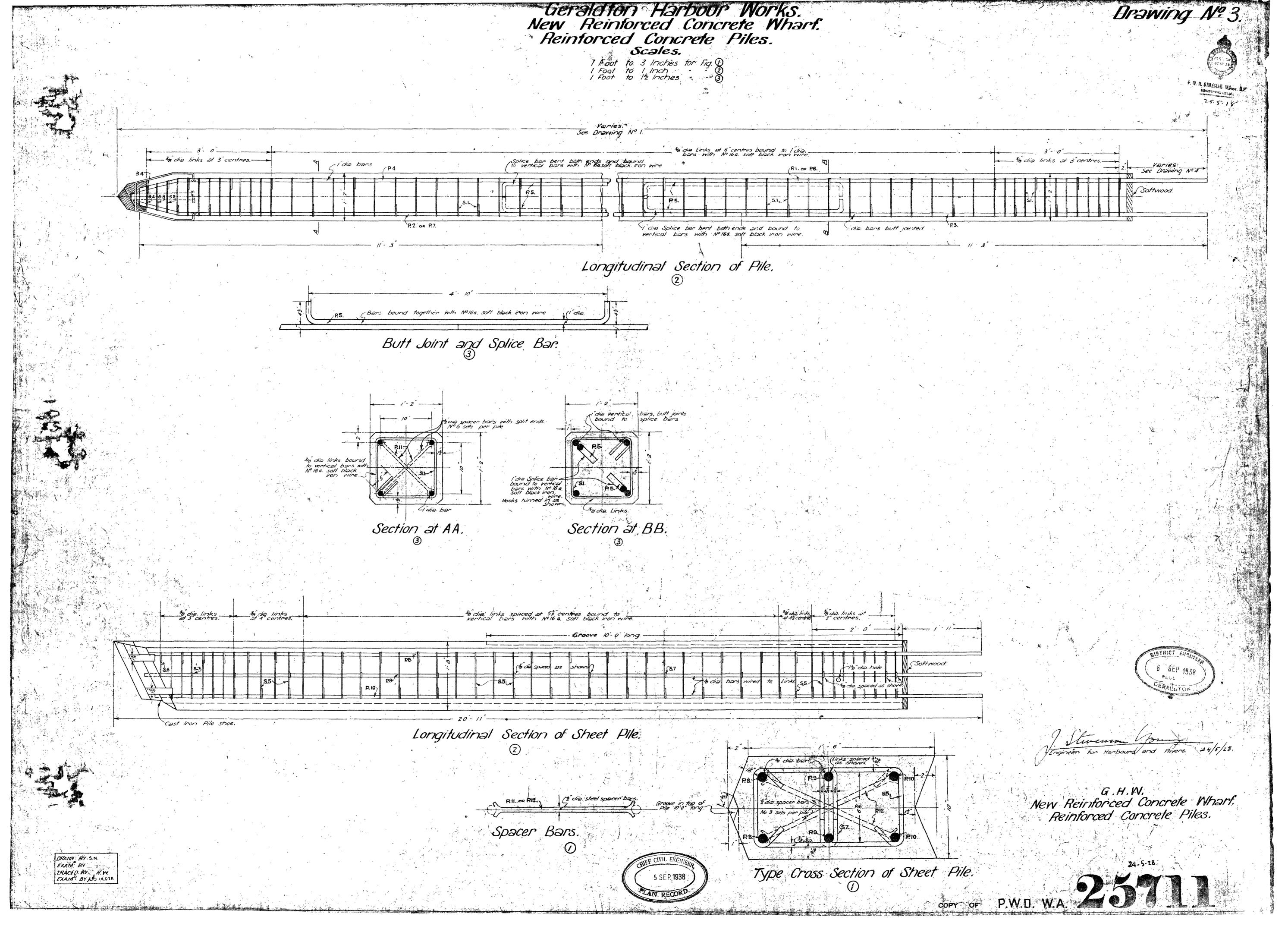
COPY of C.C.E. PLAN No.

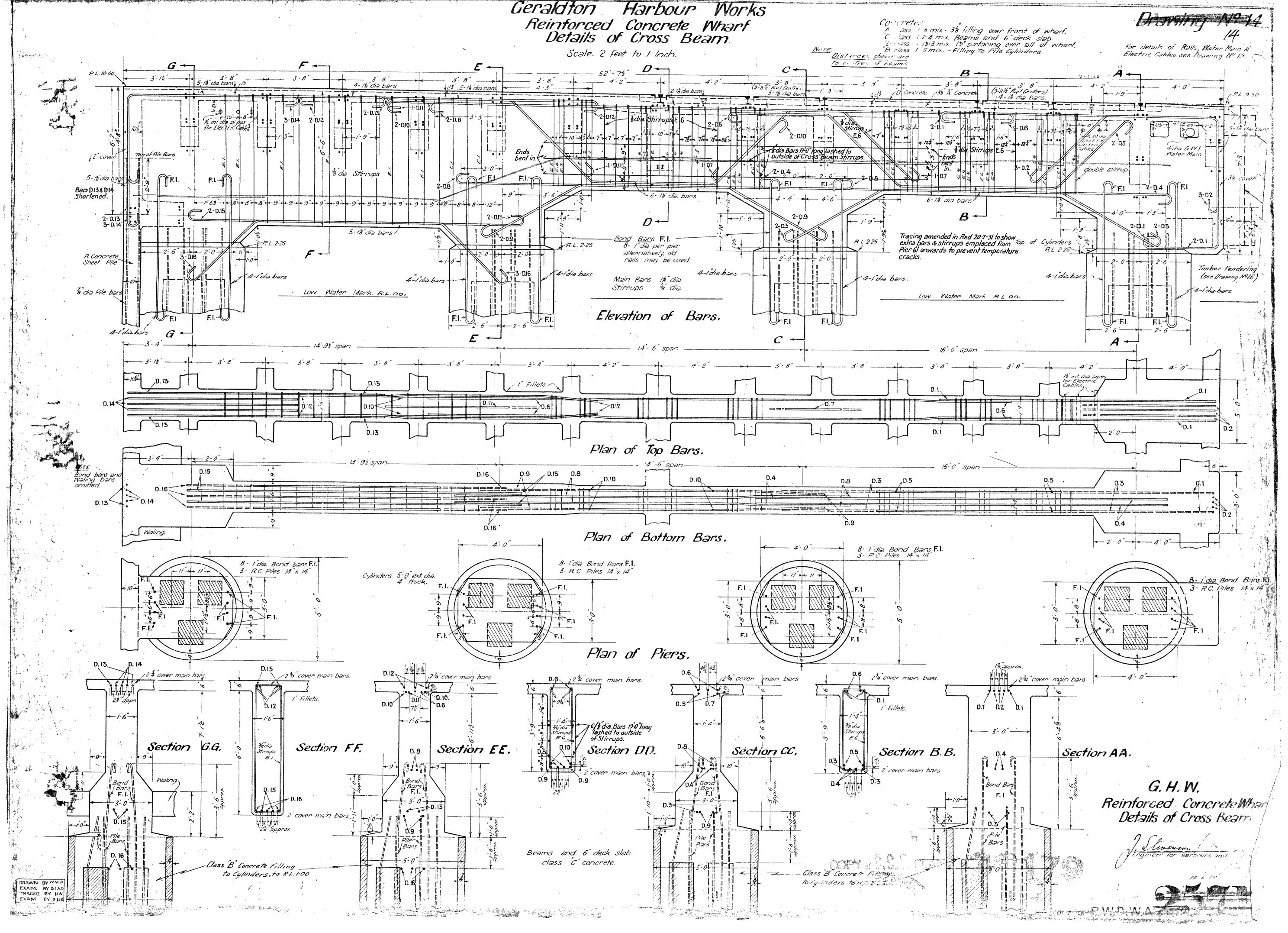
fromeer for Harbourts and R

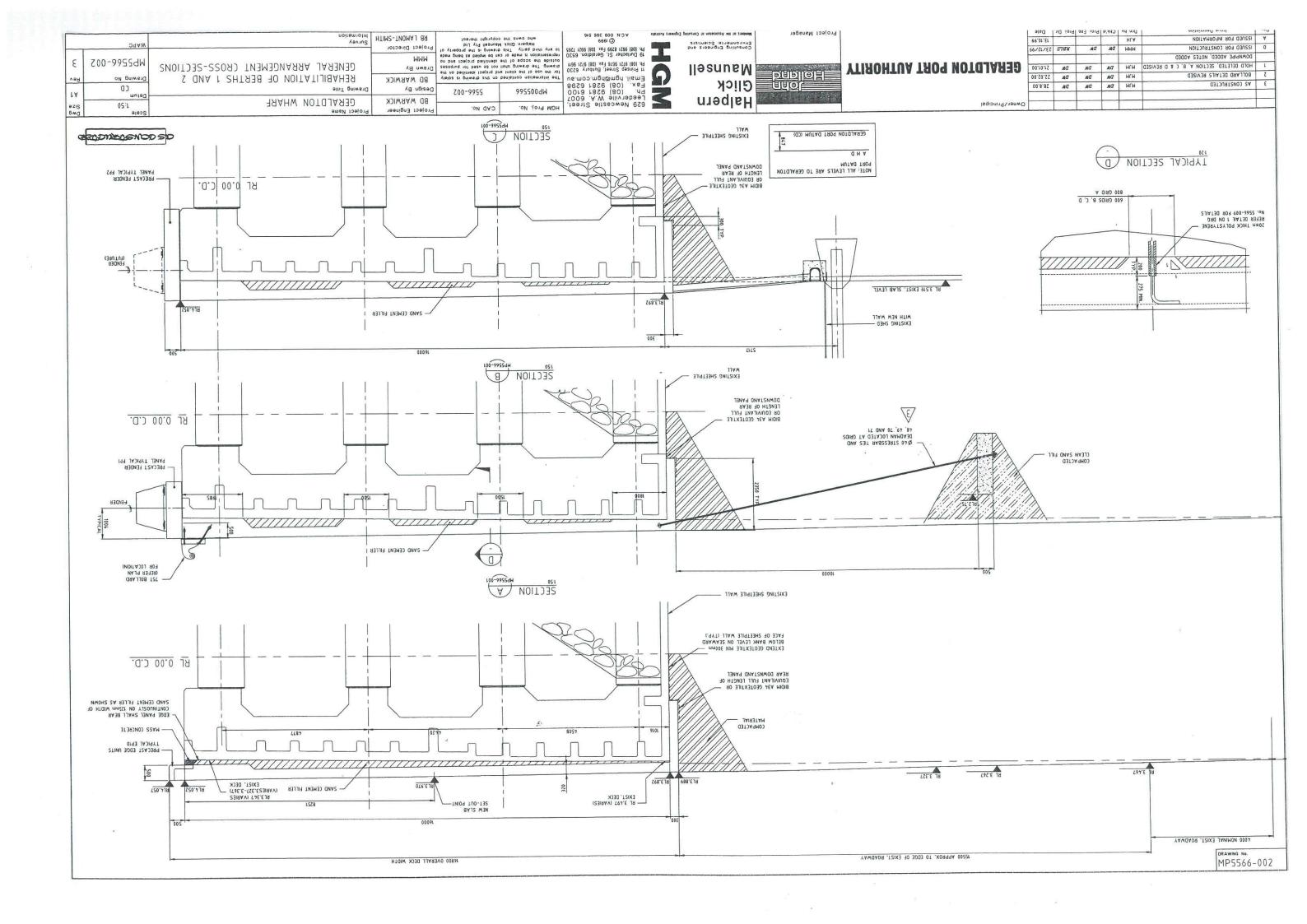
DRAWN BY A. G.A.

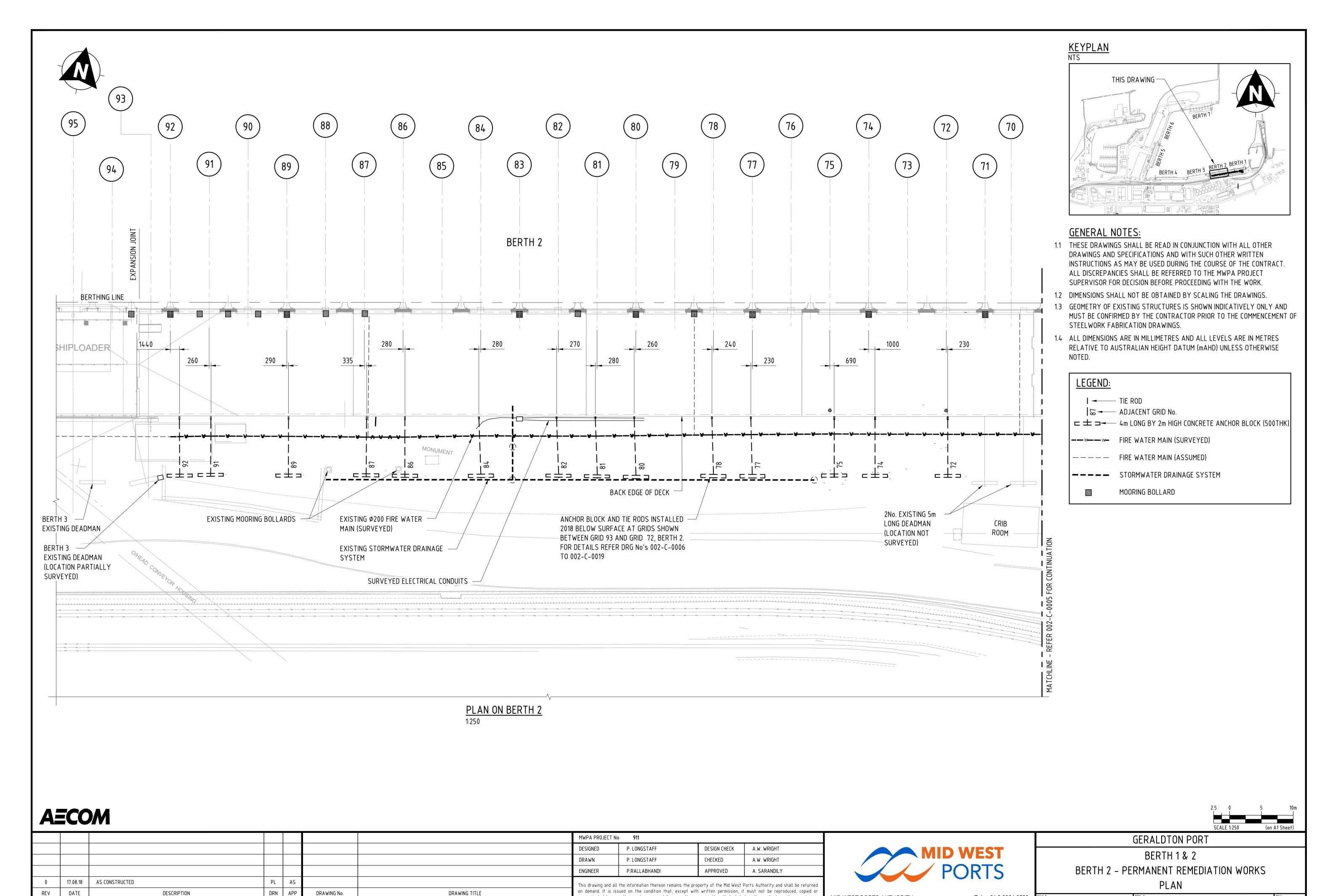
AMINED BY D. J.A. D.

BY A. E. A.









communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or

contract with which it was issued.

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298 Marine Terrace, GERALDTON 6530

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A1 - 1:250

002-C-0004

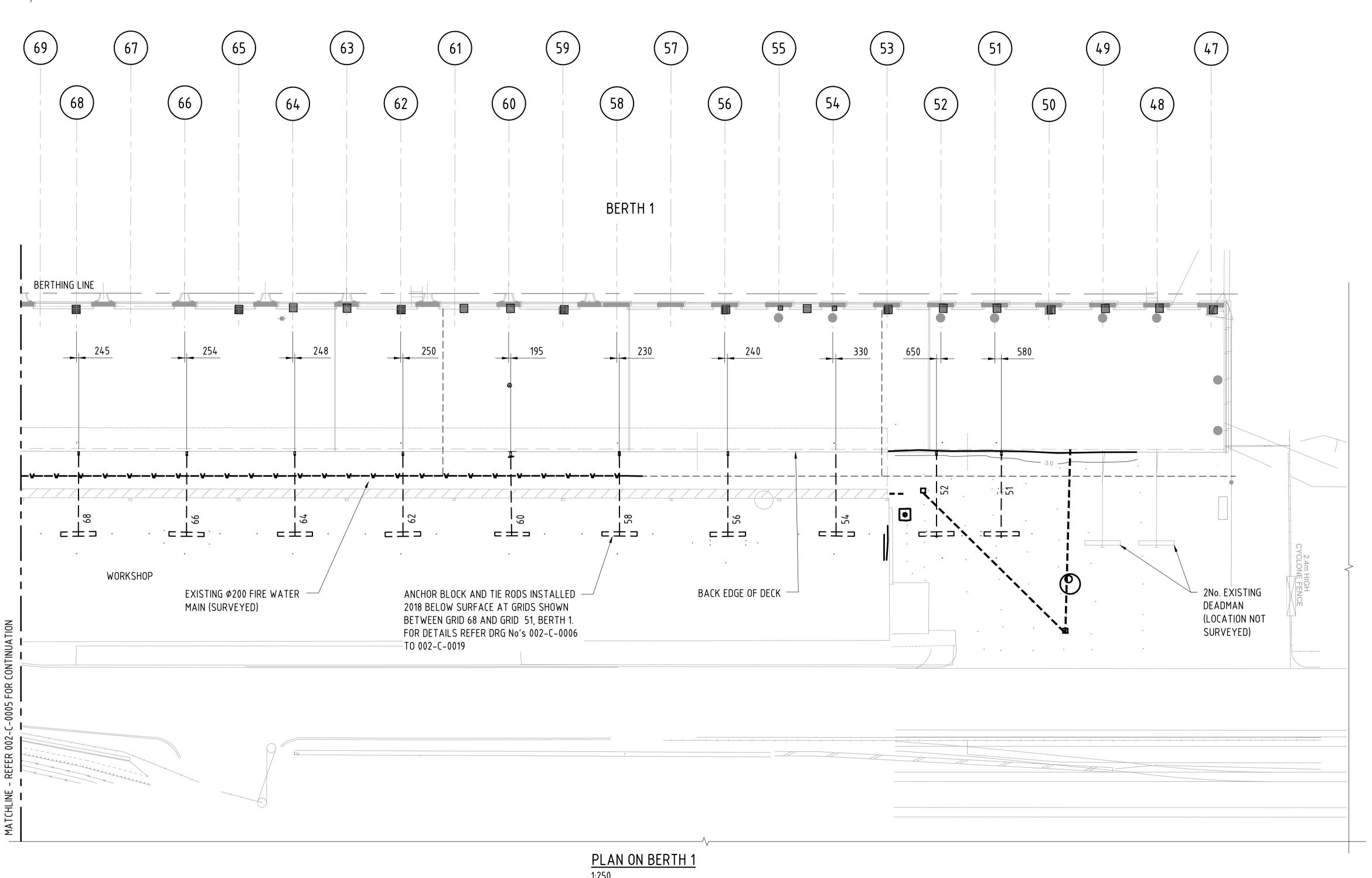
REV

REVISIONS

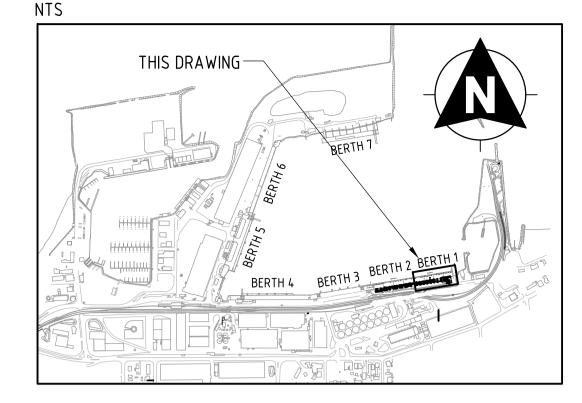
DRAWING No.

REFERENCE DRAWINGS





KEYPLAN NTS



GENERAL NOTES:

1. REFER DRG No. 002-C-0004 FOR GENERAL NOTES

AECOM

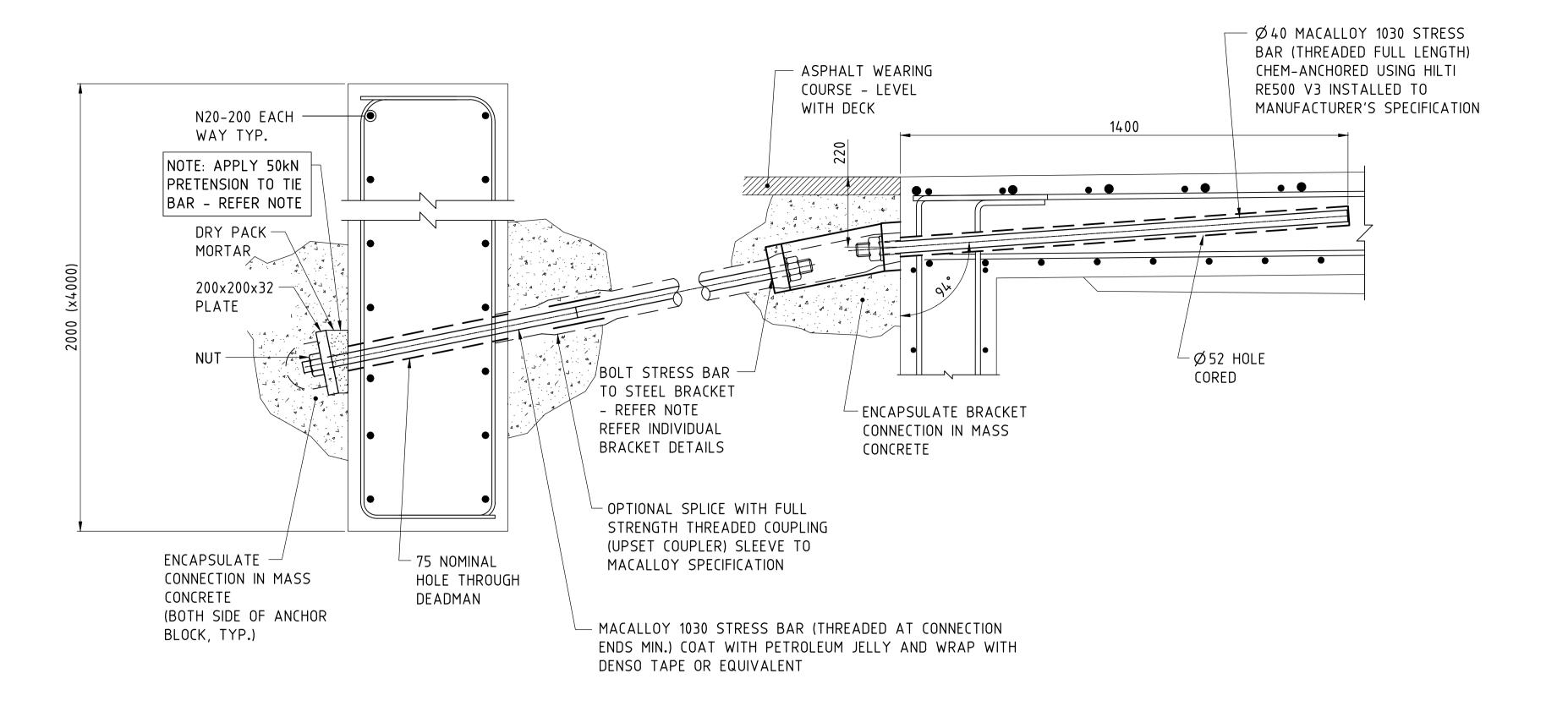
							MWPA PROJECT No: 911					
							DESIGNED	P. LONGSTAFF	DESIGN CHECK	A.W. WRIGHT		
							DRAWN	P. LONGSTAFF	CHECKED	A.W. WRIGHT		
							ENGINEER	P.RALLABHANDI	APPROVED	A. SARANDILY		
0	29.08.18	AS CONSTRUCTED	PL	AS			This drawing and a	This drawing and all the information thereon remains the property of the Mid West Ports Authority and shall be returned on demand. It is issued on the condition that, except with written permission, it must not be reproduced, copied or communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or				
REV	DATE	DESCRIPTION	DRN	APP	DRAWING No.	DRAWING TITLE	on demand. It is					
REVISIONS				·	REFERENCE DRAWINGS			contract with which it was issued.				



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		SCALE 1:250	(on A1 She						
	GERALDTON PORT	•							
	BERTH 1 & 2								
	BERTH 1 - PERMANENT REMEDIATION WORKS								
	PLAN								
LE	A1 - 1:250	002-C-0005	REV.						



DEADMAN TIEBACK DETAIL

NOTE - NUT TENSIONING

TORQUE OF 444 NEWTON METRES SHALL BE APPLIED TO EITHER THE NUT BEHIND THE PRECAST BLOCK, OR THE NUT AT THE WHARF END.

444Nm IS EQUAL TO A FORCE OF:

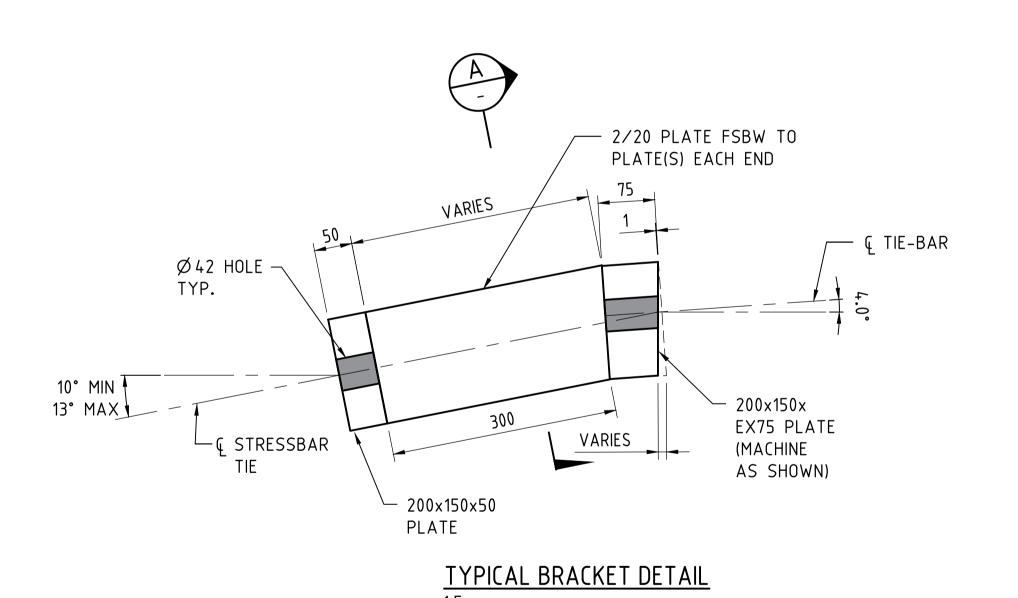
- 90.5kg AT 0.5m RADIUS, OR
- 45.3kg AT 1.0m RADIUS, OR
- 30.2kg AT 1.5m RADIUS.

AECOM

REVISIONS

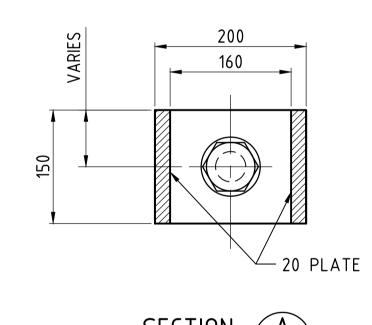
THE DIRECTION OF THE FORCE IS PERPENDICULAR TO THE WRENCH CENTRELINE. THE NUT THREADS SHOULD BE FREE OF DELETERIOUS MATERIAL AND BE GREASED TO FREELY TURN.

NOTE: THIS TORQUE DOES NOT GET APPLIED TO THE CHEM-ANCHORED BAR NUT, THIS NUT SHOULD BE DONE UP SNUGLY.



communicated to any other party, nor used for any other purpose than that stated on the particular order, enquiry, or

contract with which it was issued.



50 0 100 200mm SCALE 1:5 (on A1 Sheet)

100 0 200 400mm SCALE 1:10 (on A1 Sheet)

							MWPA PROJECT No: 911			
							DESIGNED	P. LONGSTAFF	DESIGN CHECK	A.W. WRIGHT
							DRAWN	P. LONGSTAFF	CHECKED	A.W. WRIGHT
							ENGINEER	A.W.WRIGHT	APPROVED	A. SARANDILY
0	17.08.18	AS CONSTRUCTED	PL	AW			This drawing and all the information thereon remains the property of the Mid West Ports Authority and shall be returned on demand. It is issued on the condition that, except with written permission, it must not be reproduced, copied or communicated to any other party, per used for any other purpose that stated on the particular order, enquiry, or			
REV	DATE	DESCRIPTION	DRN	APP	DRAWING No.					

REFERENCE DRAWINGS

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NOTES:

002-C-0015, MP5566-000 & MP5566-021.

APPROVED EQUIVALENT.

1. THIS DRAWING TO BE READ IN CONJUNCTION WITH AS BUILT DRAWINGS 002-C-0006 TO

3. STEEL REINFORCEMENT SHALL COMPLY WITH AS 4671 GRADE D500N.

4. STEEL PLATE SHALL BE MINIMUM GRADE 250 COMPLYING WITH AS 3678.

2. CONCRETE BACKFILL SHALL BE 15MPa AROUND ANCHOR BLOCKS AND 25MPa AROUND BRACKETS.

5. STEEL BRACKET PAINT TREATMENT - BLAST CLEAN CLASS 2 1/2 500 DFT INTERZONE 954 OR

GERALDTON PORT

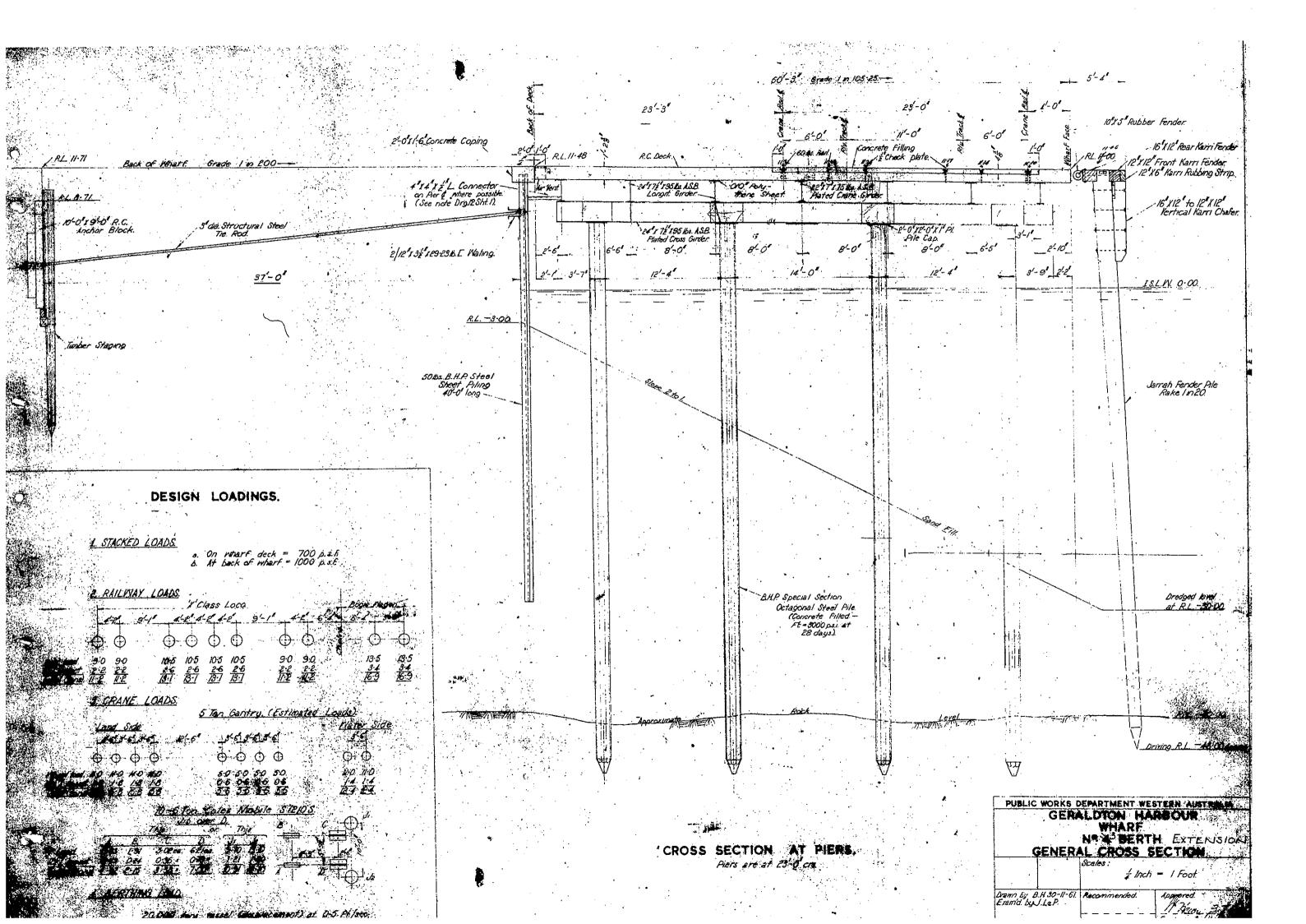
BERTH 1 & 2

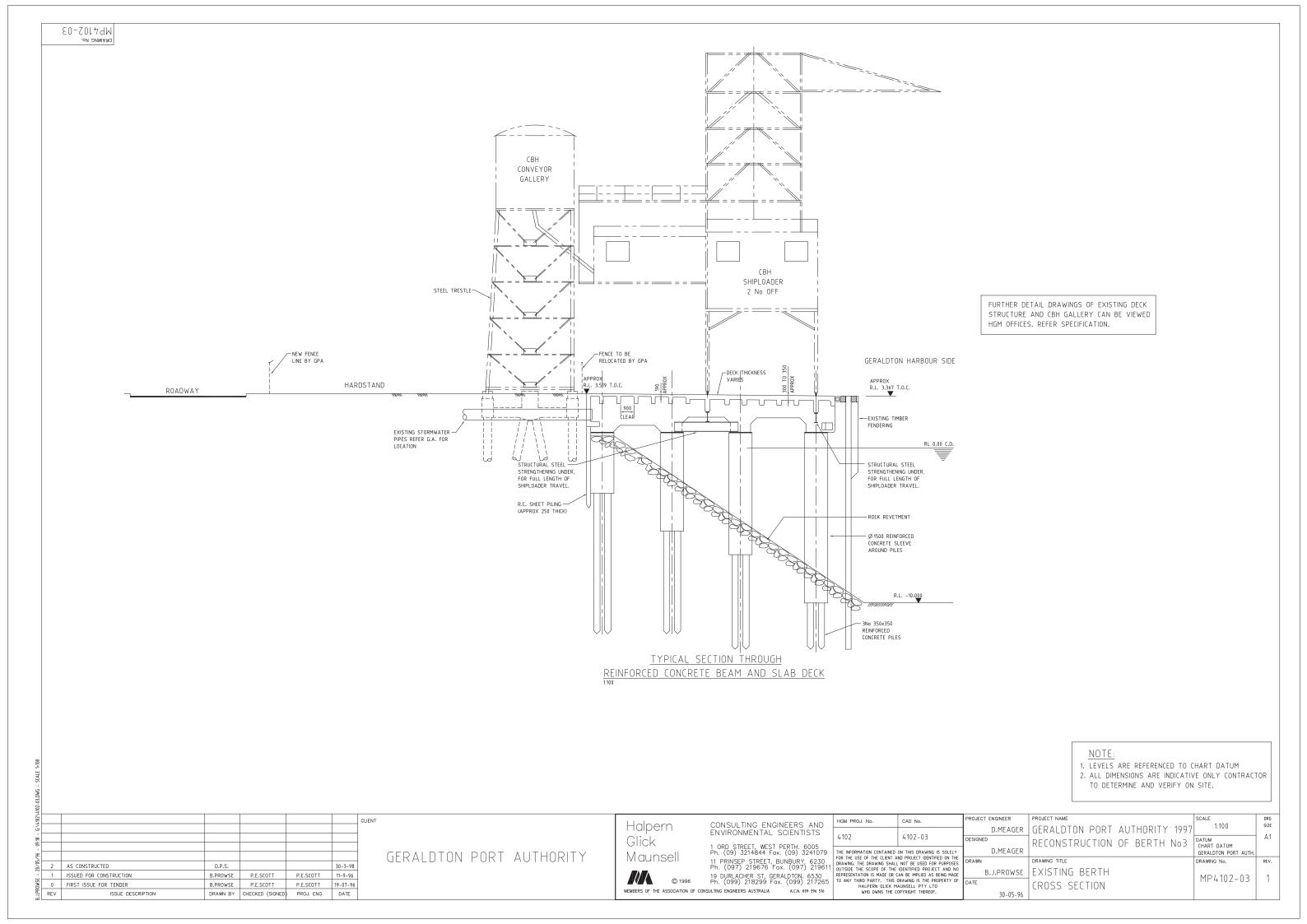
PERMANENT REMEDIATION WORKS

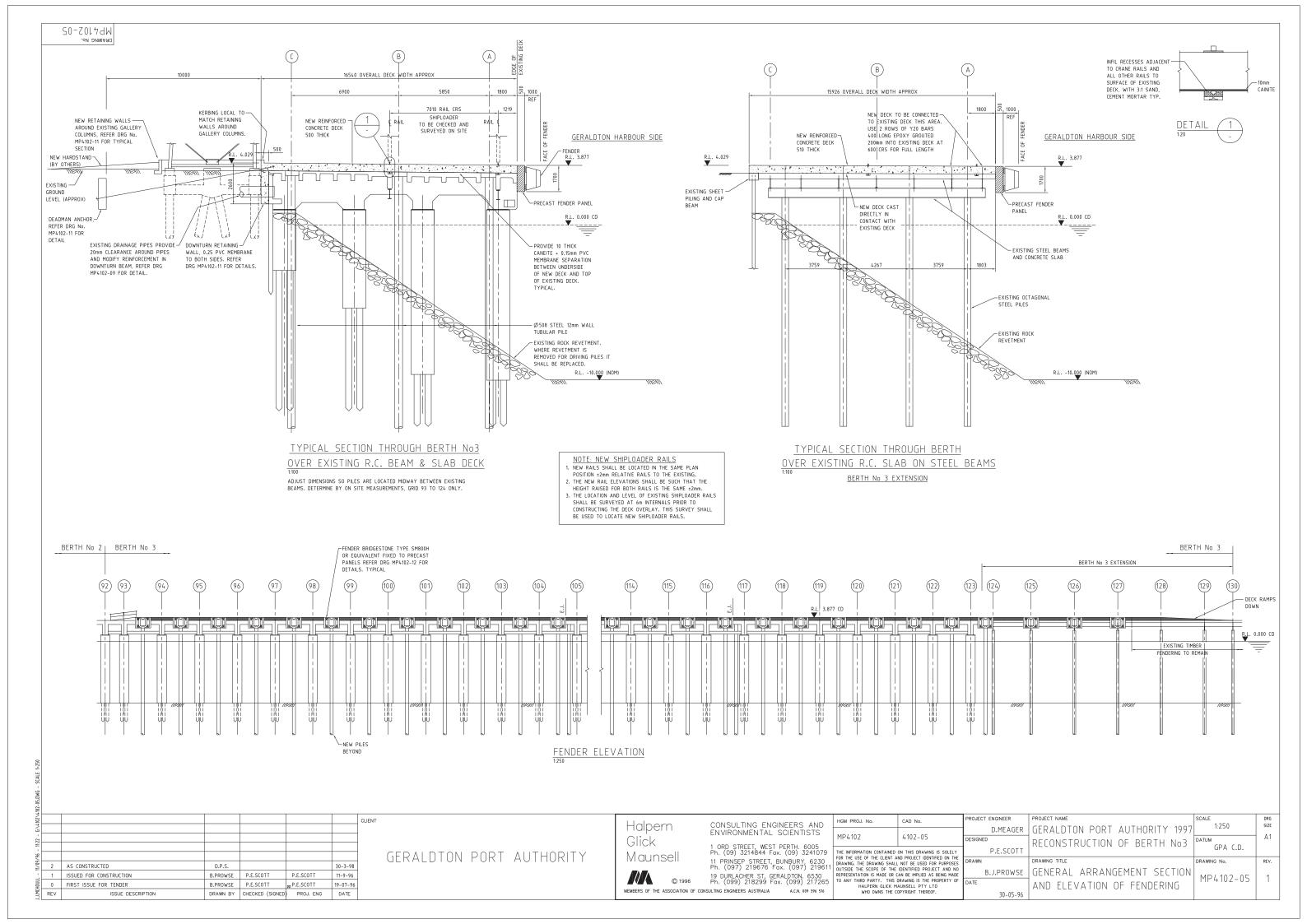
TIE ROD DETAILS

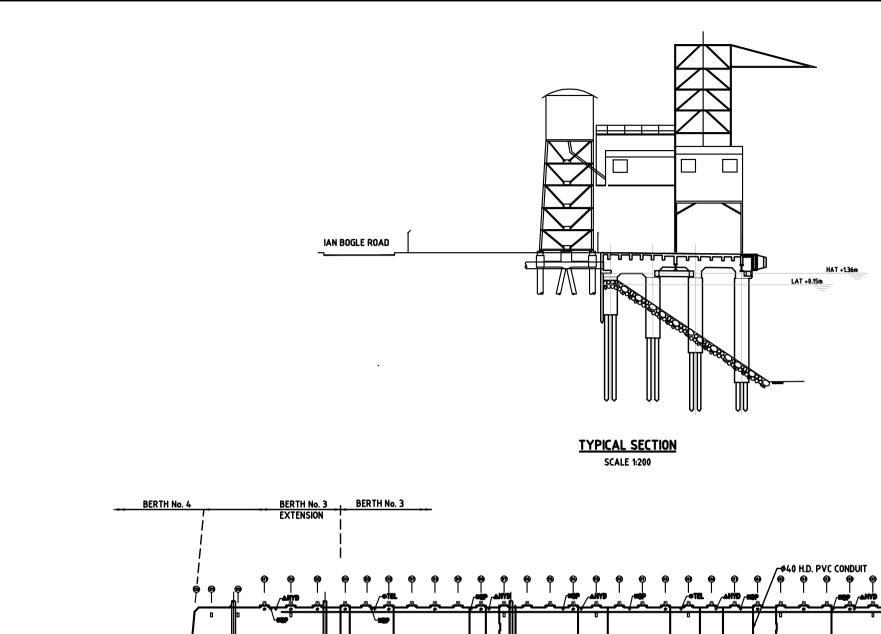
A1 - AS SHOWN

DRG. No. 60554034-SK017

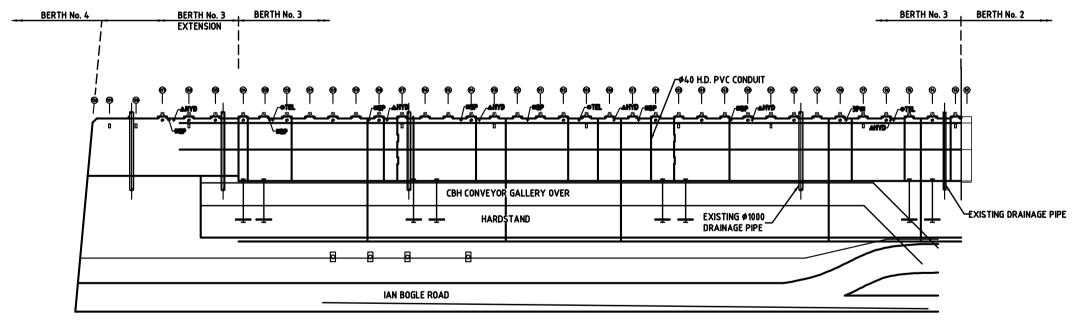








A1



SERVICES PLAN

SCALE 1:500



LEGEND:

125¢ H.D. ELECTRICAL PVC
CONDUITS IN CENTRE OF DECK

MOORING BOLLARD LOCATION

THIS DRAWING HAS BEEN REDUCED

--- EXISTING WATER PIPE

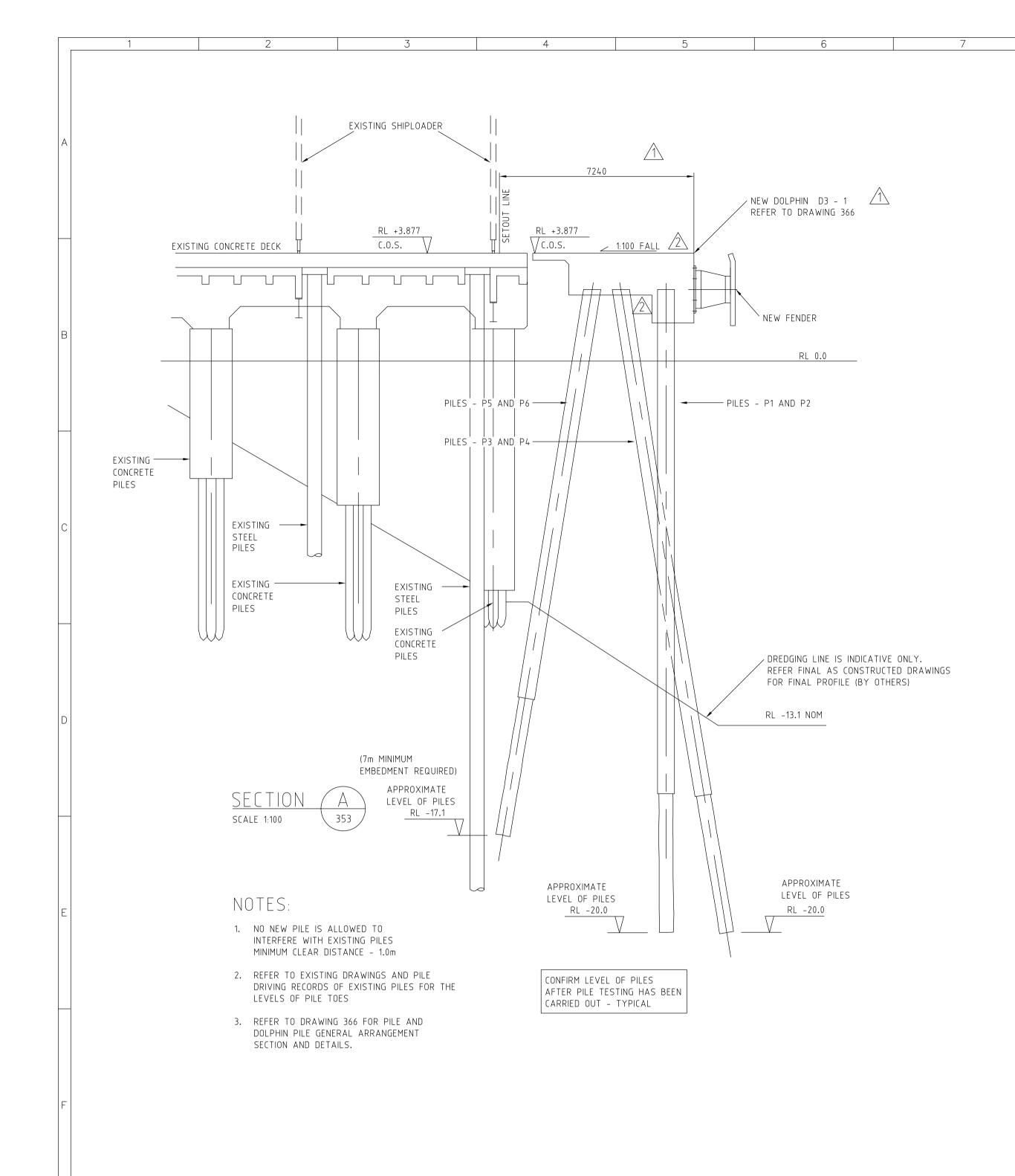
"---" EXISTING BOUNDARY FENCE

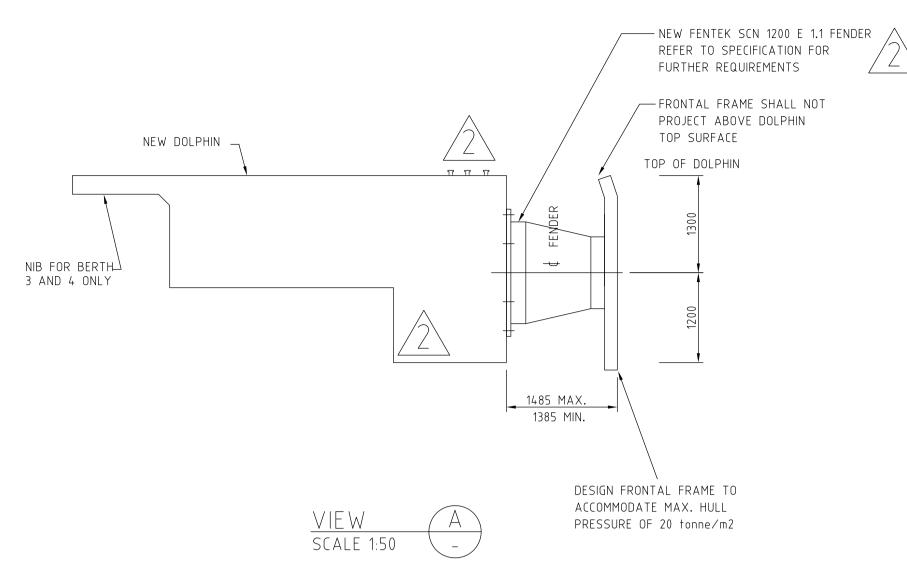
HYDRANT RECESS

3 PHASE POWER RECESSTELSTRA

EXISTING PILED BOLLARD

\vdash							Client:		Project:	Drawn	Signed	Date	Drawing Title:	CW Project No.	
					Connell Wagner		100 m			C.B.				A177-26	
									WHARF SPECIFICATION	Designed	Signed	Date	GERALDTON HARBOUR BERTH No.3	Scale	——II
					Connell Wagner Pty Ltd ABN 54 005 139 873	Telephone: +61 08 9223 1500		GERALDTON		N/A			GENERAL ARRANGEMENT	2care	
C 10.01.	1.02	FINAL ISSUE	IN		4th Floor, 207 Adeliade Tce, Perth	Facsimile: +61 08 9325 9948			BOOKLET	Verified	Signed	Date	GENERAL ARRANGETERI	AS SHOWN	I/
B 10.04.	4.01	ADDED TIDE LEVELS TO ELEVATION	DPH		Western Australia, 6004, Australia	Email: cwper@hutch.com.au		PORT AUTHORITY		l c.v.					
A 02.11.	1.00	ISSUE FOR CLIENT REVIEW	C.B.		A person using Connell Wagner drawings and other data accepts the	e risk of:				Approved	Signed	Date	1	Drawing No.	Kev.
Rev. Date		Revision Details	Ву	Ver. Арр.	accuracy against the original hard copy versions; using the drawings or other data for any purpose not agreed to	o in writing by Connell Wagner.				K.H.				C - 002	C





SUPPLY AND INSTALL HOLDING DOWN BOLTS AS PER FENDER MANUFACTURER'S RECOMMENDATIONS FENDER ANCHOR POSITIONS CONFIRM WITH FENDER MANUFACTURER BEFORE CASTING VIEW B Anchor Bolts for Fender

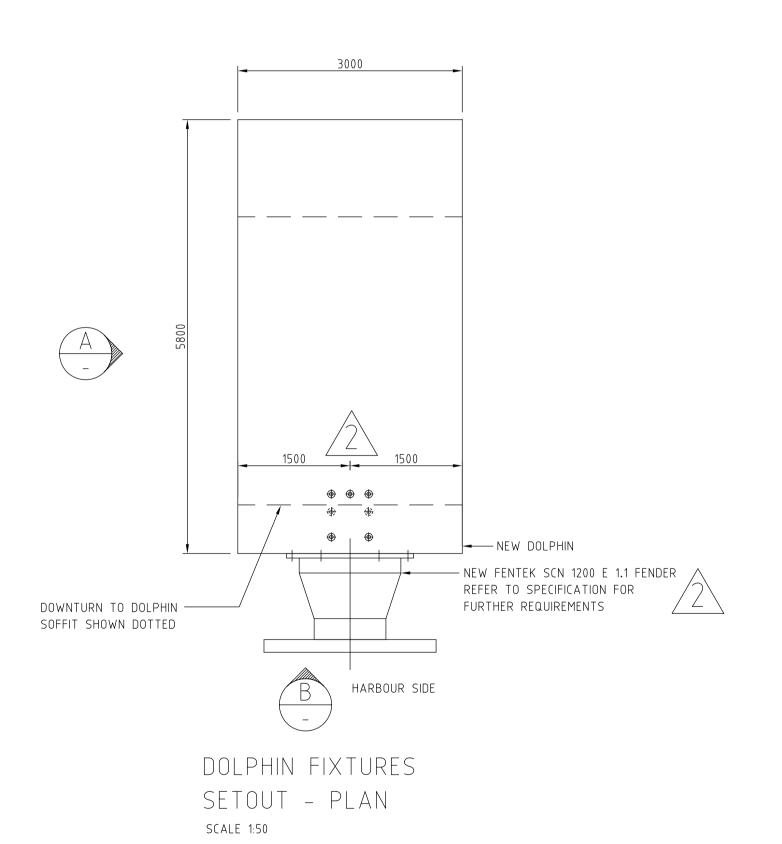
NOTE: FENDER OMITTED FOR CLARITY

NOTES:

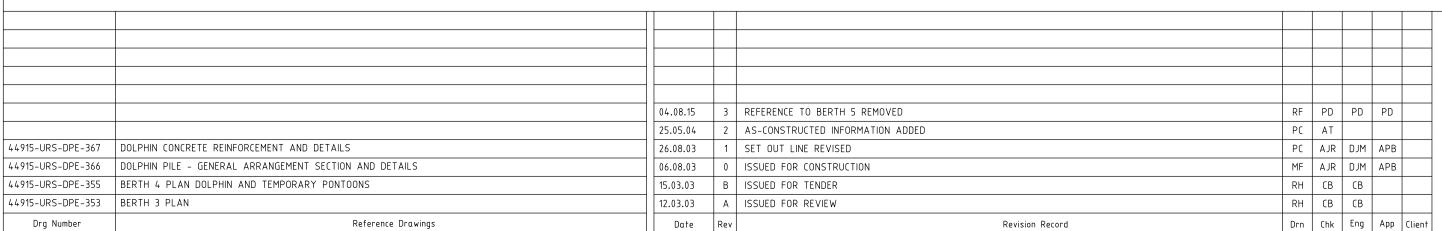
- CONFIRM LOCATION OF HOLDING DOWN BOLTS/ANCHORS, BLOCKOUTS WITH CAPSTAN'S MANUFACTURER BEFORE CASTING ON SITE
- CONFIRM LOCATION OF ANCHOR/HOLDING DOWN BOLTS FOR FENDER WITH THE FENDER'S MANUFACTURER BEFORE CASTING ON SITE
- 3. FRONTAL FRAME COATING:
 AS PER MANUFACTURER'S RECOMMENDATIONS

MINIMUM REQUIREMENTS:
BLASTING GRADE: SSPC-SP-10 OR SIS Sa21/2
PRIMARY COATING: ZINC RICH PRIMER -- 70 MICRONS
FINAL COATING: HIGH BUILD HIGH SOLIDS EPOXY -- 2 x 200 MICRONS
TOTAL DRY FILM THICKNESS: MIN. 450 MICRONS (BLACK)

4. CAST-IN FERRULES FOR ATTACHMENT OF ANY FRONTAL FRAME CHAINS NOT SHOWN. IF REQUIRED CAST-IN FERRULES TO BE TO MANUFACTURER'S RECOMMENDATIONS AND APPROVED BY SUPERINTENDENT.



AS—CONSTRUCTED



LEVEL 3, HYATT CENTRE,
20 TERRACE ROAD
EAST PERTH, WA 6004
Telephone: (08) 9221 163
Facsimile: (08) 9221 163

MF AJR DJM APB

RH CB CB

Drn Chk Eng App Client It remains the property of URS Australia Pty Ltd

Facsimile: (08) 9221 1639

PLOT SCALE

1

VERTICAL DA

PORT

DESIGN BY	C. BUI	28.02.03	CLIENT
DRAWN BY	R. HOARE	28.02.03	
DRAFTING CHECK	C.B.	11.03.03	
DESIGN CHECK	N.S./M.I./A.E/W.A	11.03.03	
APPROVAL	A.P.B.	06.08.03	
FINAL APPROVAL	BY CLIENT		
			. H

PLOT SCALE

1:1

VERTICAL DATUM

PORT DATUM

CGG94

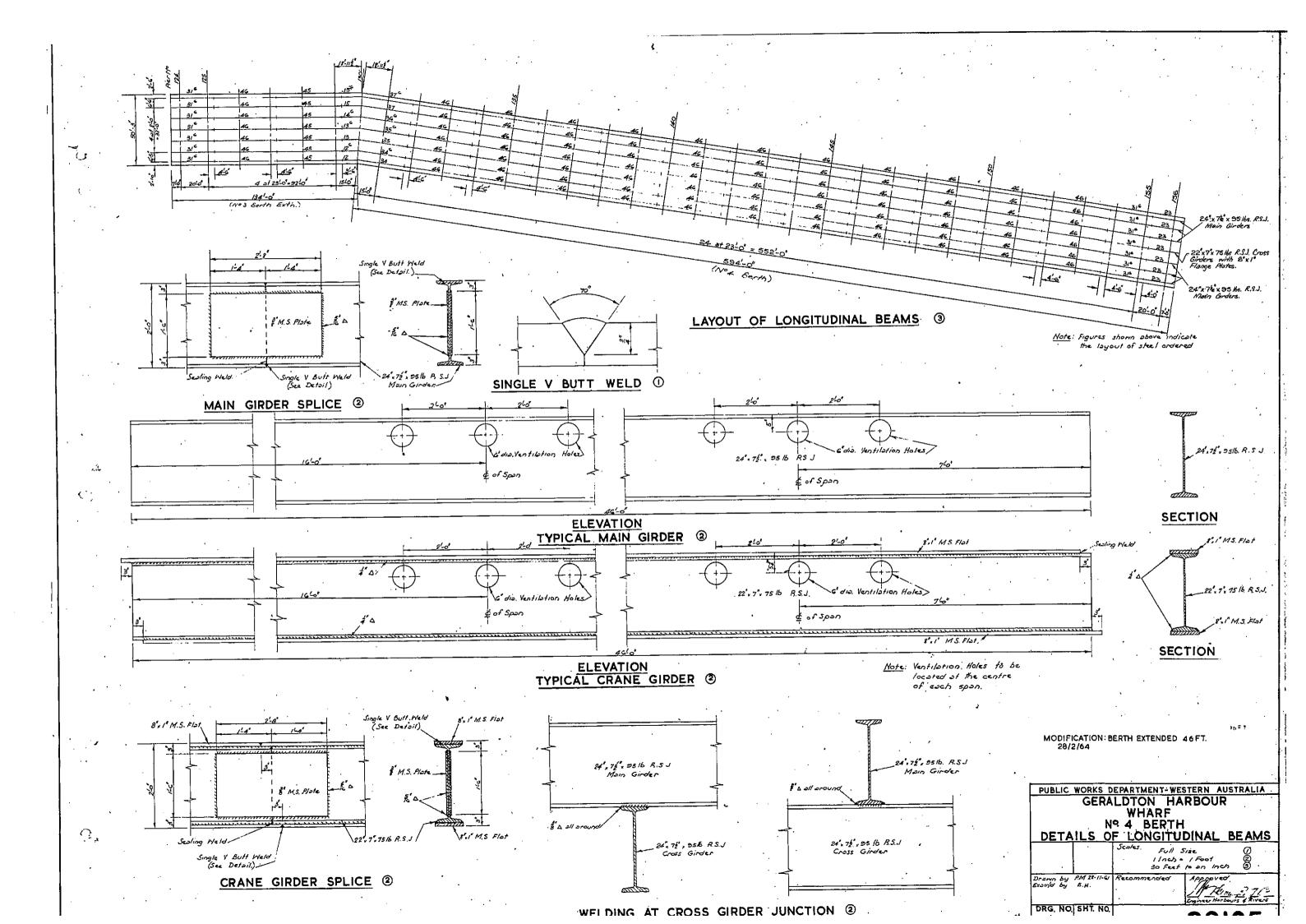


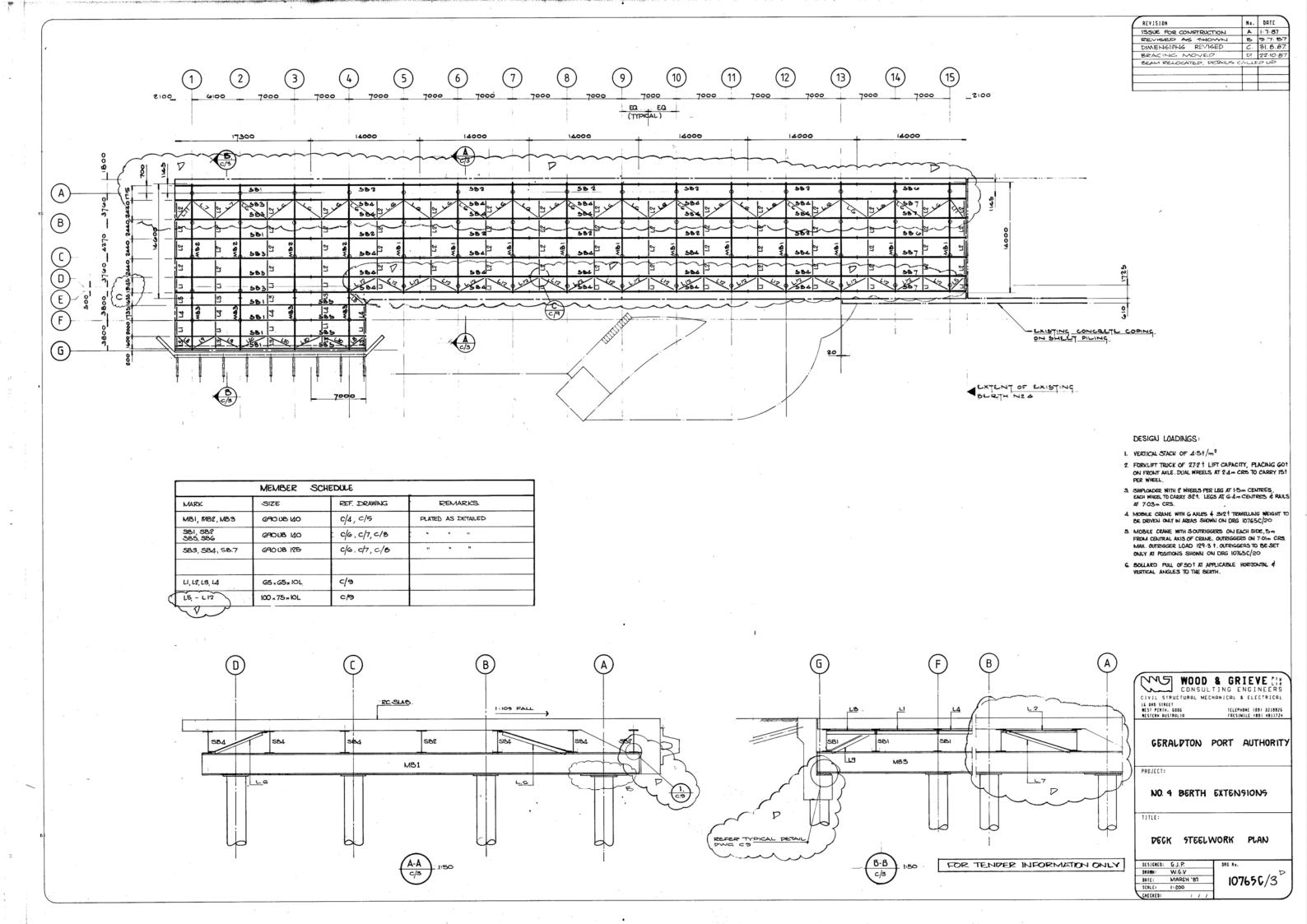
TITLE
GERALDTON PORT
ENHANCEMENT PROJECT
MODIFICATION TO BERTH 3 & 4
BERTH 3 — SECTION, DETAILS AND
DOLPHIN FIXTURES SETOUT

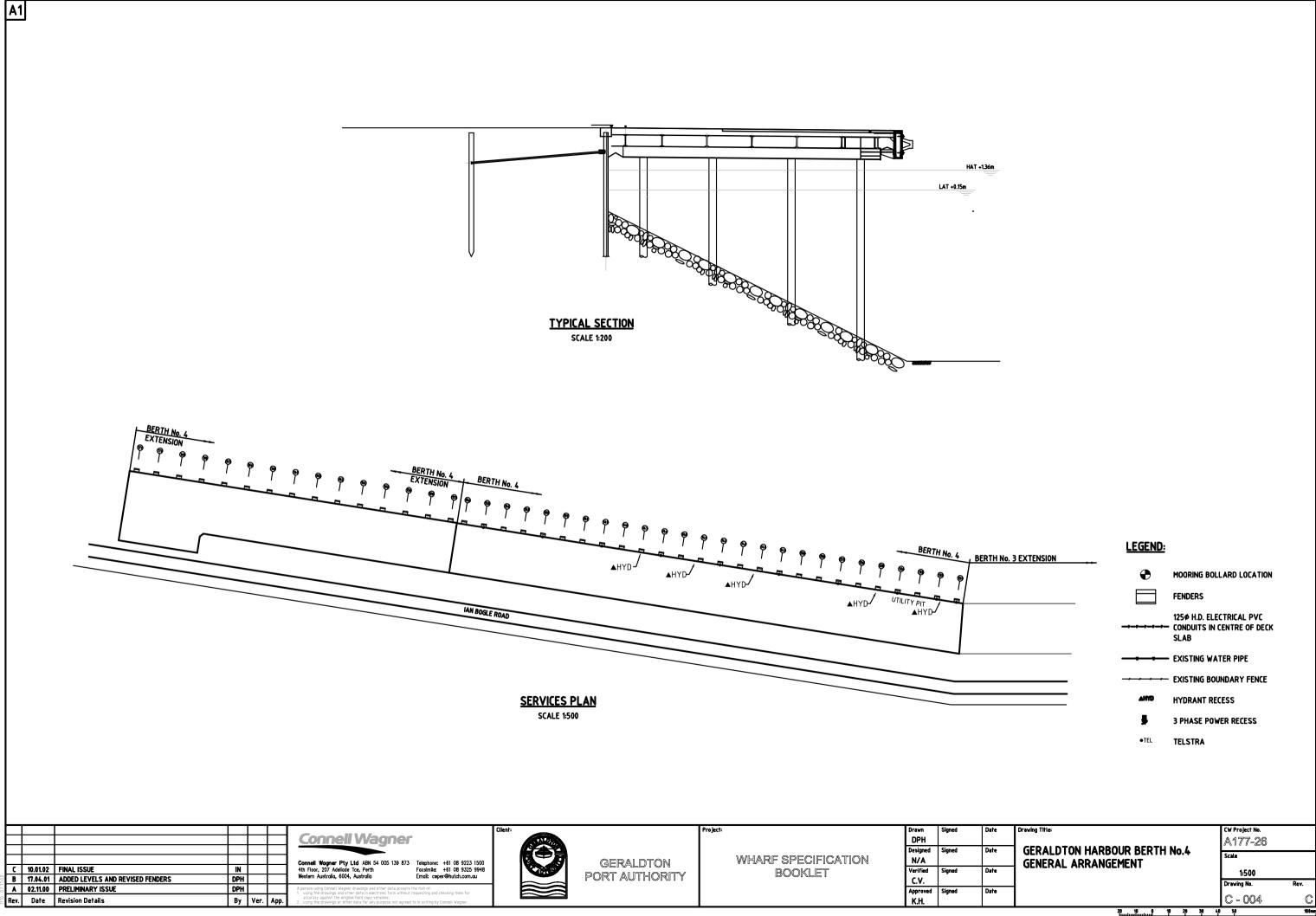
PROJECT No. | DRAWING No. | REV | 44915-004 | 44915-URS-DPE-354 | 3 | 16

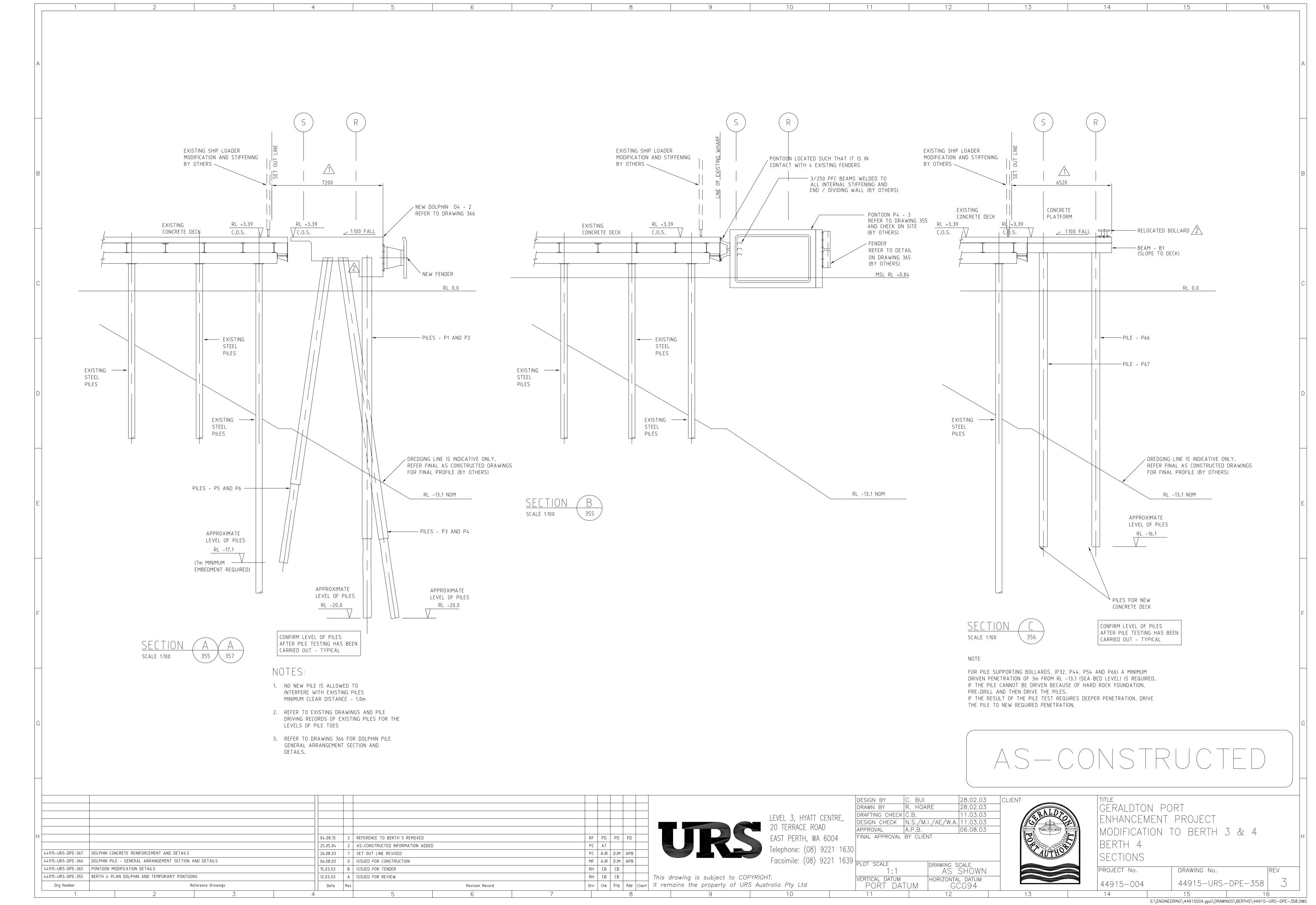
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A 1

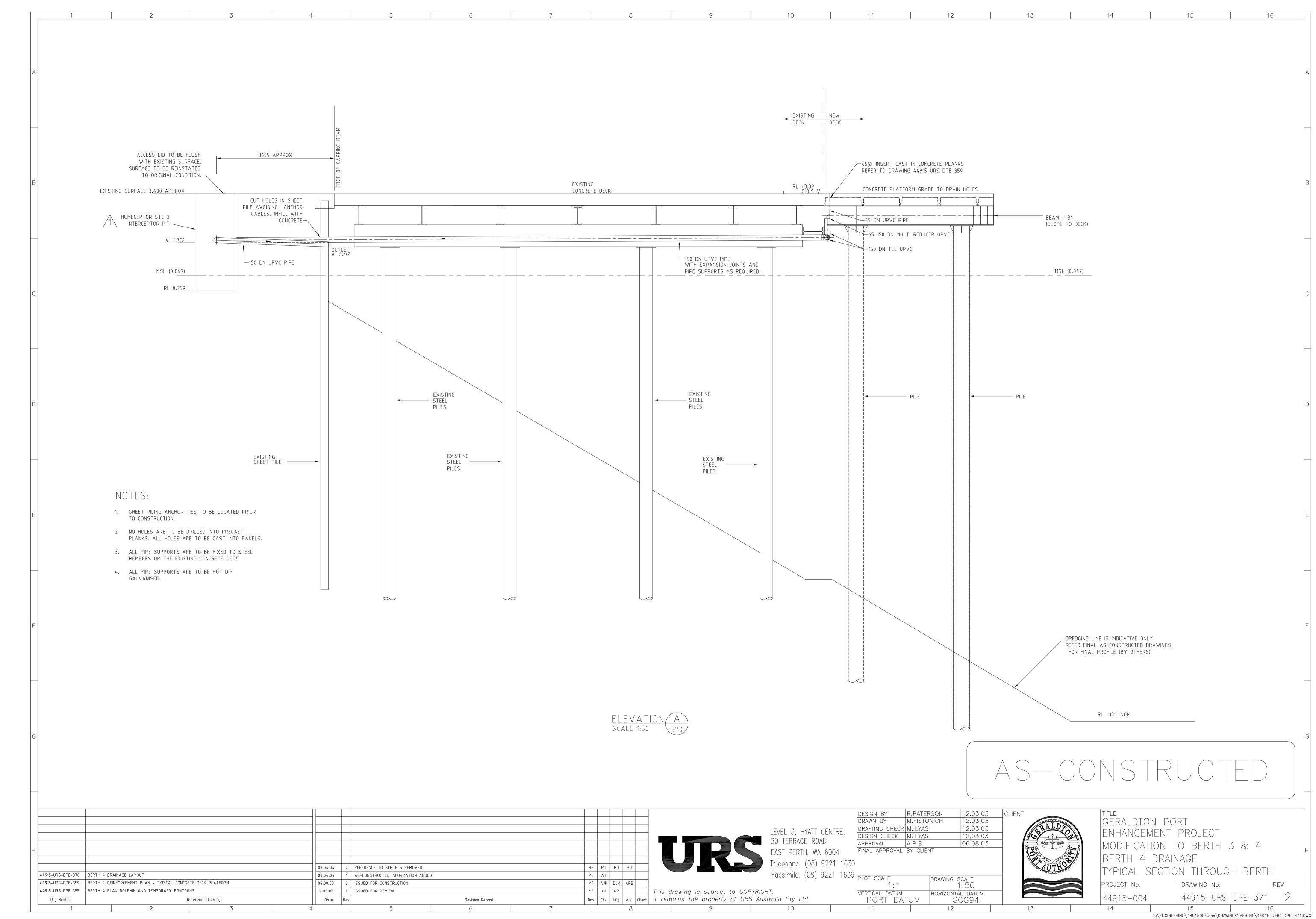




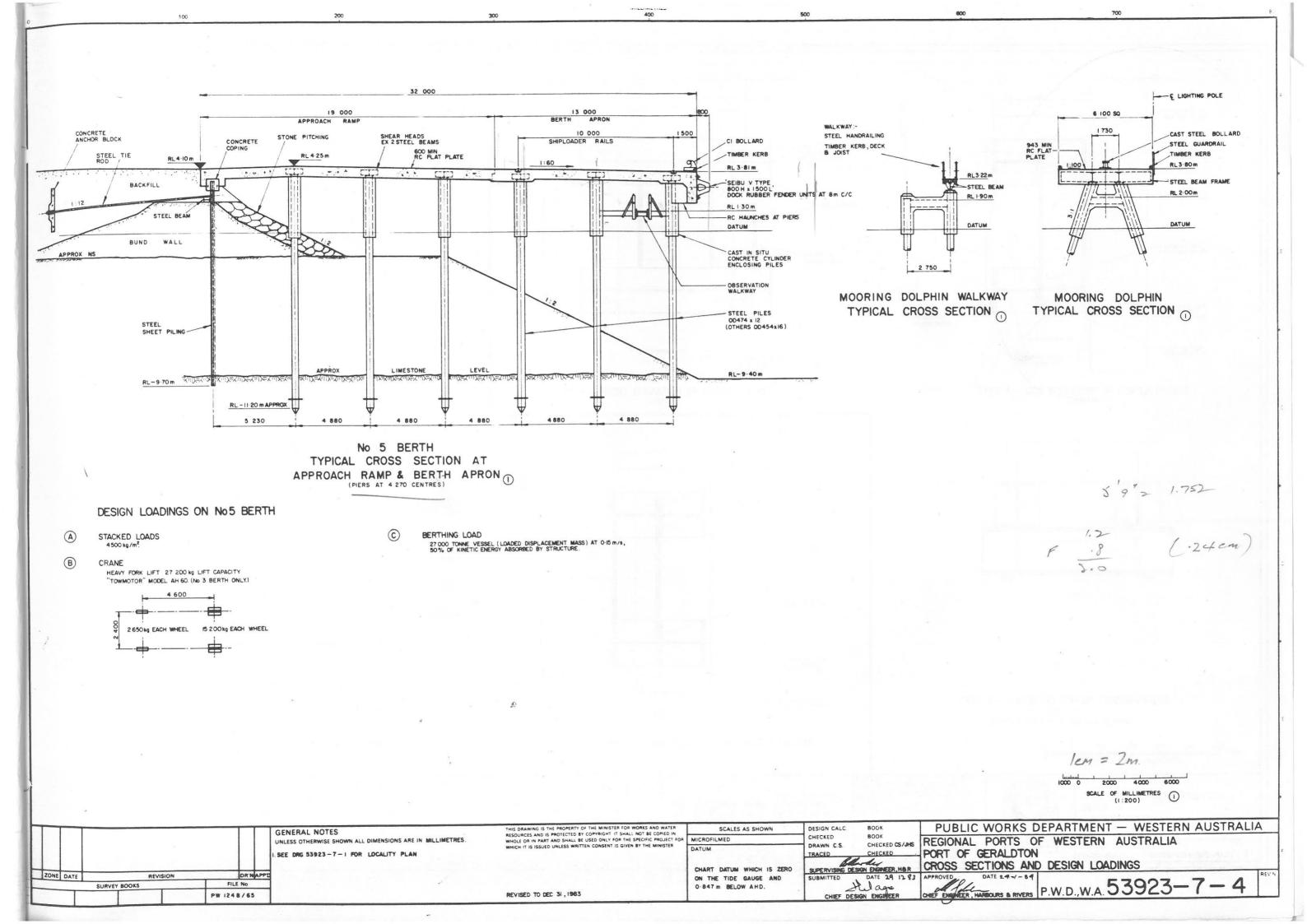




A1

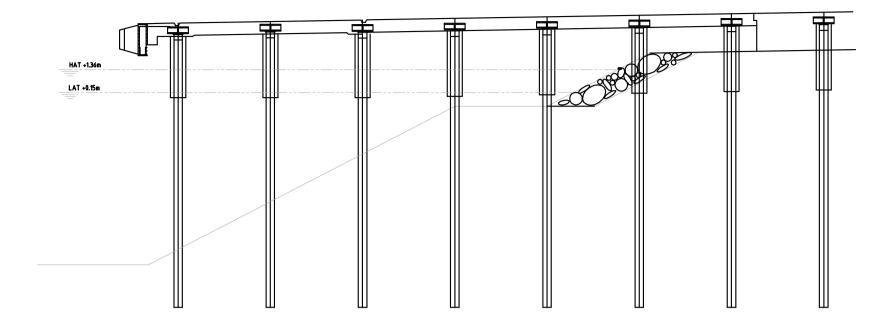


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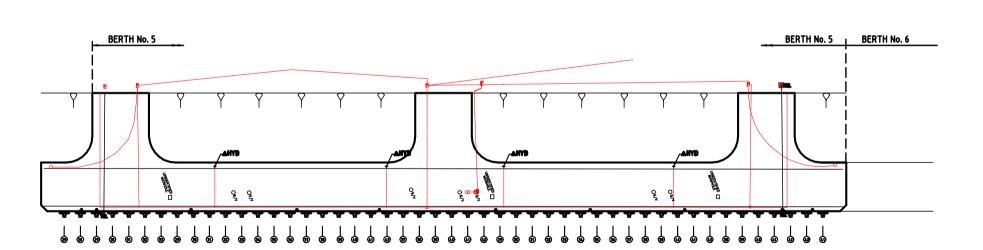








TYPICAL SECTION SCALE 1:100



SERVICES PLAN SCALE 1:500

LEGEND:

MOORING BOLLARD LOCATION

FENDERS

1250 H.D. ELECTRICAL PVC CONDUITS IN CENTRE OF DECK SLAB

EXISTING WATER PIPE EXISTING BOUNDARY FENCE

HYDRANT RECESS

3 PHASE POWER RECESS

20 10 0 10 20 30 40 50

						Client:		Project:	Drawn	Signed	Date	Drawing Title:	CW Project No.	
					Connell Wagner	TILL OF			DPH				A177-26	
									Designed	Signed	Date	☐ GERALDTON HARBOUR BERTH No.5	71111 00	
					Connell Wagner Pty Ltd ABN 54 005 139 873 Telephone: +61 08 9223 1500		GERALDTON	WHARF SPECIFICATION	N/A	""		GENERAL ARRANGEMENT	Scale	
С	10.01.02	FINAL ISSUE	IN		4th Floor, 207 Adeliade Tce, Perth Facsimile: +61 08 9325 9948			BOOKLET	Verified	Signed	Date	- APHENAL ANNAHAPHENT	1:500, 1:100	
8 B	17.04.01	REVISED DRAWING No. & NOTES	DPH		Western Australia, 6004, Australia Email: cwper⊕hutch.com.au		PORT AUTHORITY		l cv	1 -				
				 	A				<u> </u>				Drawing No.	Rev.
<u> Α</u>	92.11.90	ISSUE FOR INFORMATION	L.B.		using the drawings and other data in electronic form without requesting and checking them for				Approved	Signed	Date			
≅ Rev.	Date	Revision Details	Ву	Ver. App.	accuracy against the original hard copy versions; 2. using the drawings or other data for any purpose not agreed to in writing by Connell Wagner.				K.H.				C - 006	\mathbb{C}

SUMMARY OF DESIGN LOADS

NOTE: DESIGN LOADS APPLIES TO BOTH BERTH NO.5 & BERTH NO. 6 UNLESS OTHERWISE NOTED.

> REFER TO "MARINE STRUCTURES" SPECIFICATION FOR DESIGN AND CONSTRUCTION FOR DETAIL DESIGN CRITERIA. ABBREVIATED CRITERIA AS BELOW.

1. VERTICAL DEAD LOADS

1.1 <u>CONCRETE</u> – SELF WEIGHT BASED ON A CONCRETE DENSITY OF

25t/m3

1.2 <u>STEELWORK</u> – 7.85 t/m3

1.3 <u>ALUMINUM</u> – 2.70 t/m3

2. VERTICAL LIVE LOADS

REFER CONNELL WAGNER REPORT "WHARF SPECIFICATION BOOKLET COMMERCIAL SHIPPING HARBOUR GERALDTON PORT AUTHORITY" JANUARY 2002 REFERENCE A177-26 REVISION C

2.1 <u>DOLPHINS</u>

5 kPa LIVE LOAD:

2.2 <u>WALKWAYS</u>

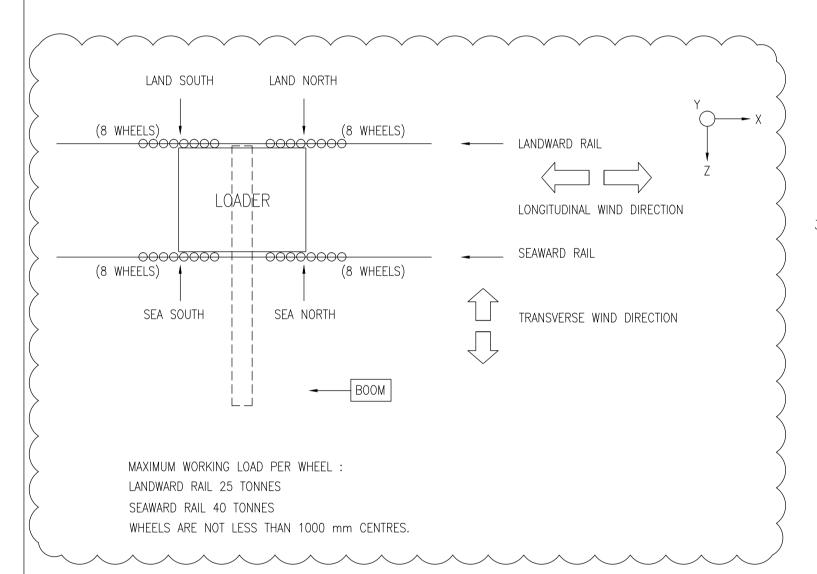
2.5 kPa, 1.5kN POINT LOAD LIVE LOAD:

2.3 <u>SHIPS MOBILE GANGWAY PLATFORMS</u>

LIVE LOAD: 3 kPa

SHIPS' GANGWAY NOT TO BE LANDED DIRECTLY ON TROLLEY, A "SHIP'S BROW" BETWEEN SHIP'S GANGWAY AND TROLLEY SHALL BE USED.

2.4 <u>SHIPLOADER LOADS</u>



3. HORIZONTAL LOADS

3.1 VEHICLE BRAKING LOADS

ALL VEHICLES 30% x MASS

3.2 <u>WIND</u>

THE DETERMINATION OF LOADS INDUCED BY WIND ARE BASED ON

THE FOLLOWING CONDITIONS: OPERATIONAL WIND LOADS

IMPORTANCE LEVEL 3

REGION B, TERRAIN CATEGORY 1

MOORING AND FENDER LEAN ON FORCES V = 32 m/sec 30 sec GUSTOPERATING SERVICEABILITY V = 23 m/sec 3 sec GUST

3.2.2 <u>NON-OPERATIONAL WIND LOADS</u>

IMPORTANCE LEVEL 3 REGION B, TERRAIN CATEGORY 2

ULTIMATE $V_{1000} = 60 \text{ m/sec } 3 \text{ sec GUST}$

3.3 <u>WAVE</u>

NOT CRITICAL

3.4 <u>SEISMIC FORCES</u>

LOADS WILL BE DETERMINED IN ACCORDANCE WITH AS1170.4 AND AS1170.0 2002 APPENDIX D USING THE FOLLOWING FACTORS.

3.4.1 <u>ULTIMATE LEVEL EARTHQUAKE</u>

ANNUAL EXCEEDANCE PROBABILITY 1:1000

PROBABILITY FACTOR Kp

1.4 PEAK HORIZONTAL GROUND ACCELERATION, a 0.09 g

ADJUSTED ACCELERATION FACTOR, a

0.0126 g SITE FACTOR, S 1.25

STRUCTURE RESPONSE FACTOR Rf 4.5

IMPORTANCE FACTOR, I

3.5 <u>TEMPERATURE</u>

LOADS WILL BE DETERMINED IN ACCORDANCE WITH: AS5100:2

AMBIENT TEMPERATURE UNIFORM TEMPERATURE VARIATION 5°C TO 58°C

POSITIVE VERTICAL DIFFERENTIAL GRADIENT

: 0°C (BOTTOM SURFACE), TO -18°C (TOPSURFACE) NEGATIVE VERTICAL DIFFERENTIAL GRADIENT : 7°C (TOP SURFACE), TO -0°C (BOTTOM SURFACE)

1.0

4. BERTHING STRUCTURES

4.1 <u>DESIGN VESSEL RANGE</u>

		BULK (CARRIER	TANKER
DESIGN VESSEL — BULK CARRIER	UNITS	MINIMUM	MAXIMUM	IAINNER
DEADWEIGHT TONNAGE (DWT)	tonnes	30,000	70,000	55,000
DISPLACEMENT TONNAGE (DISP)	tonnes	40,000	90,000	72,700
LENGTH OVERALL (Loa)	metres	187	225	222
BREADTH (B)	metres	27	32.4	35
MOULDED DEPTH	metres	14.5	18	19
LADEN DRAFT (D)	metres	10.3	12.5	12.5
BALLASTED DRAFT	metres	6.2	6.5	7
BALLASTED DISPLACEMENT	tonnes	24,000	40,000	42,000
BERTHING ANGLE	degrees	(6)	6	6

4.2 <u>BERTHING VELOCITY (m/sec)</u>

30,000 BUI	K CARRIER	70,000 DWT E	BULK CARRIER	55,000 0	L TANKER
BALLAST	BALLAST LADEN		LADEN	BALLAST	LADEN
0.15	5 0.12 (0.1		0.10	0.15	0.11

ABNORMAL FACTOR (APPLIED TO NORMAL ENERGY)

30,000 BUL	_K CARRIER	70,000 DWT E	BULK CARRIER	55,000 01	IL TANKER
BALLAST	LADEN	BALLAST	LADEN	BALLAST	LADEN
1.75	1.50	1.50	1.25	1.50	1.25

4.3 <u>BERTHING ENERGIES</u>

VESSEL ABNORMAL BERTHING ENERGY 565 kNm

-1/3 POINT BERTHING FOR 30,000 DWT VESSEL

-1/4 POINT BERTHING FOR 70,000 DWT VESSEL -1/4 POINT BERTHING FOR 55,000 DWT VESSEL

FENDER SHALL MEET THE FOLLOWING CHARACTERISTICS:

MAXIMUM RATED DEFLECTION 72% MINIMUM RATED ENERGY 570 kNm

MAXIMUM RATED REACTION 1300 kN

RATED ENERGY AND RATED REACTION INCLUDE TEMPARATURE, TOLERANCE AND ANGULAR CORRECTION FACTORS IN ACCORDANCE WITH PIANC.

MAXIMUM STRUCTURE LOAD AT FENDER LOCATIONS IS 1689 KN (SERVICEABILITY).

4.4 <u>FRICTION</u>

COEFFICIENT OF FRICTION BETWEEN THE SHIP'S HULL AND THE

FENDER PANEL: $\mu = 0.3$ MAXIMUM

4.5 <u>CONTACT PRESSURE</u> MAXIMUM PRESSURE BETWEEN THE SHIP'S HULL AND THE FENDER

BULK CARRIER = 200kPa

PANEL:

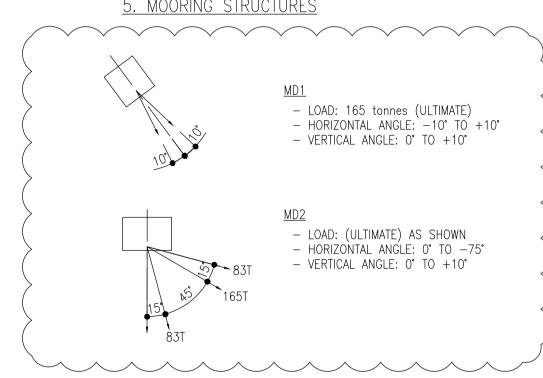
4.6 <u>APPROACH ANGLE</u> MAXIMUM ANGLE OF APPROACH WHEN BERTHING: 6° FROM

BREASTING LINE

4.6 ROPE ANGLES VERTICAL : -10° TO +25° DEGREES HORIZONTAL : 0° TO 10° DEGREES

LOAD : 113t (ULTIMATE)

5. MOORING STRUCTURES



6. CORROSION ALLOWANCE

STEEL STRUCTURES BELOW SEABED STEEL STRUCTURES BETWEEN SEABED 0.0 AND -0.5m C.D : 1 mm STEEL STRUCTURES BETWEEN 0.5m AND 2.0m C.D : 2 mm STEEL STRUCTURES ABOVE 2.0m C.D : 1 mm

CORROSION ALLOWANCE IS NOT APPLIED TO THE INTERNAL SURFACES OF HOLLOW STRUCTURAL STEEL SECTIONS AS THESE WILL BE SPECIFIED TO BE SEALED AND HAS NOT BEEN APPLIED TO HANDRAILS AND

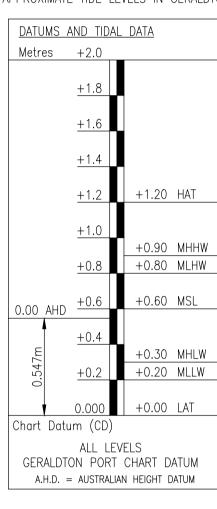
7. DESIGN LIFE

DESIGN LIFE FOR STRUCTURES: 40 YEARS

HANDRAILS AND GRATING WILL HAVE A NOMINAL DESIGN LIFE OF 10 YEARS, ASSUMING REGULAR ROUTINE MAINTENANCE AND PERIODIC

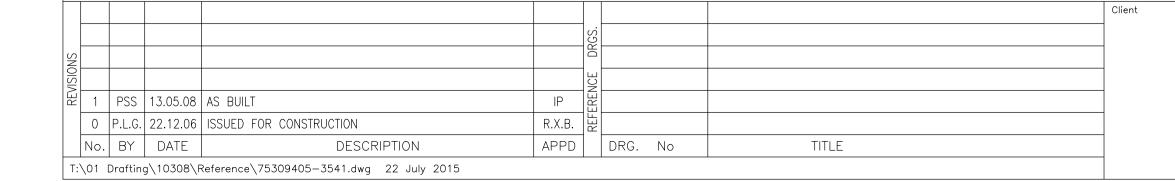
8. TIDES

APPROXIMATE TIDE LEVELS IN GERALDTON HARBOUR ARE AS FOLLOWS:



AS CONSTRUCTED

75309405-3541





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The signing o	drawing is confidential and shall only of this title block confirms the design cked in accordance with the Maunsell	be used for the n and drafting of	purposes of this project. This project have been prepared
ESIGNED	I.J.P.	CHECKED	I.J.P.

DESIGNED	I.J.P.	CHECKED	I.J.P.
DRAWN	J.L.	CHECKED	P.M.
APPROVED	R.X.B.	DATE	06.10.06
Datum		Survey	

MAUNSELL	AECOM
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Maunsell Australia Pty Ltd

Level 1, 629 Newcastle Street

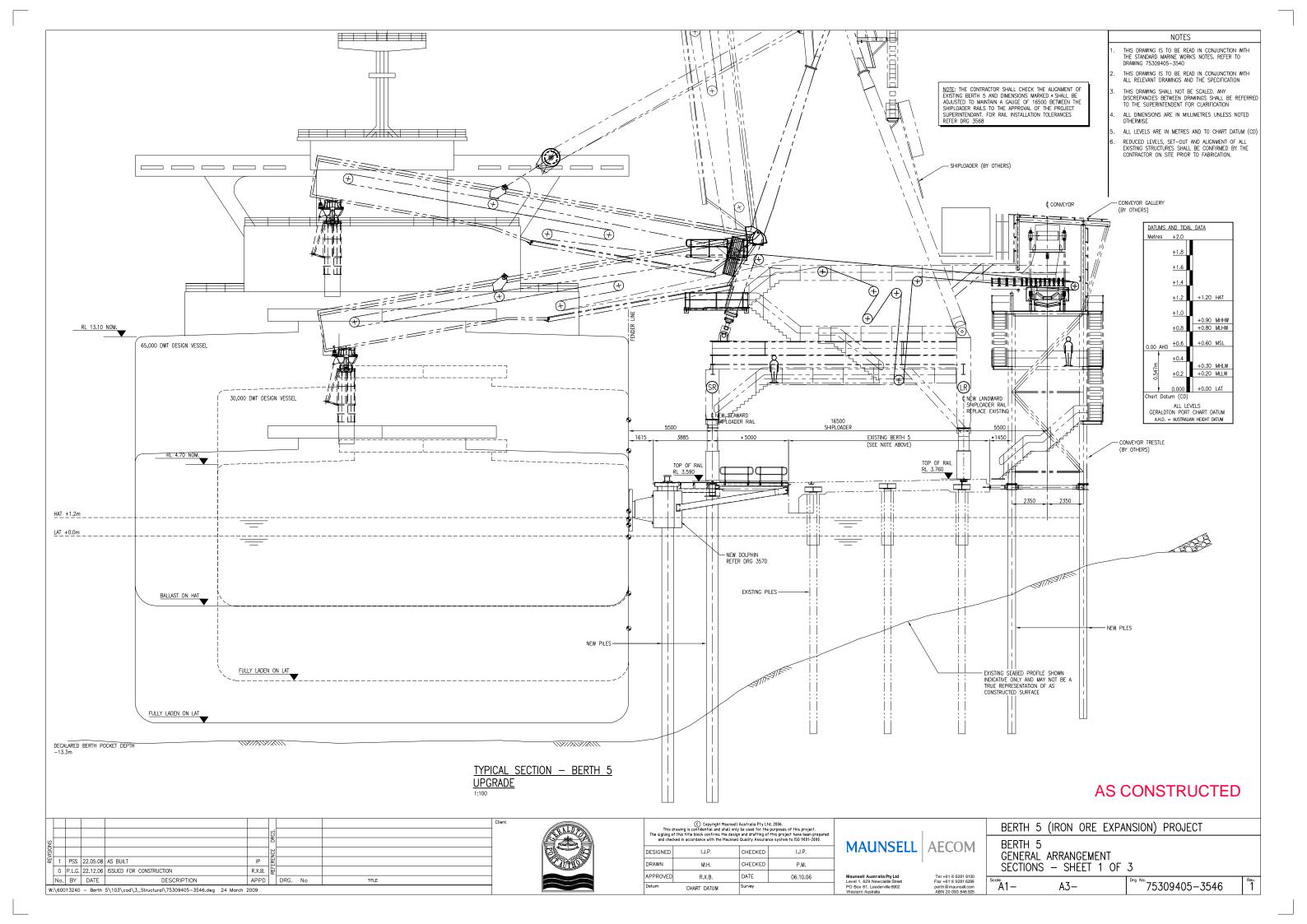
PO Box 81, Leederville 6902

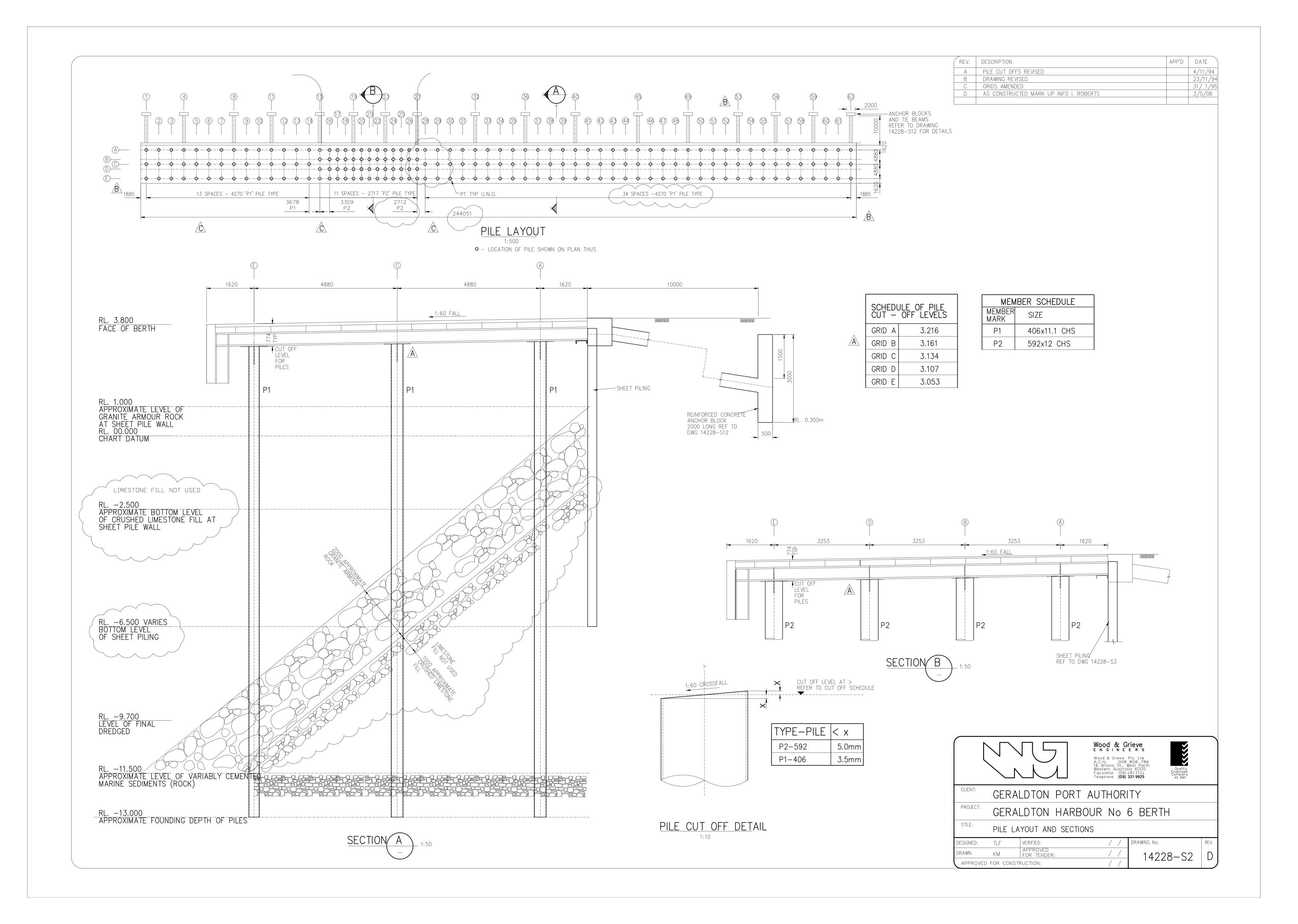
Western Australia

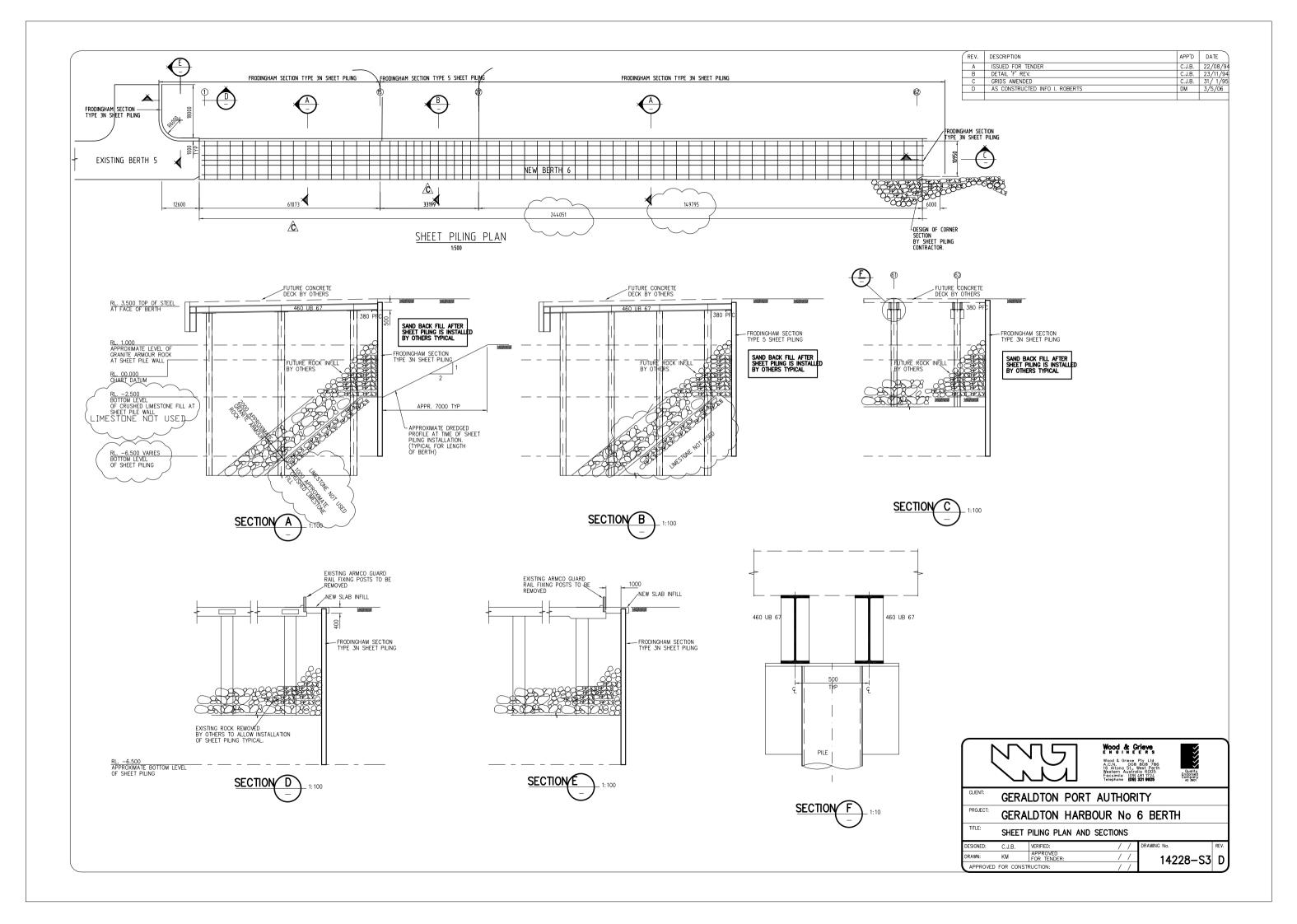
Tel +61 8 9281 6100
Fax +61 8 9281 6299
perth@maunsell.com
ABN 20 093 846 925

BERTH 5 (IRON C	DRE EXPANSION)	PROJECT
BERTH 5 DESIGN CRITERIA		

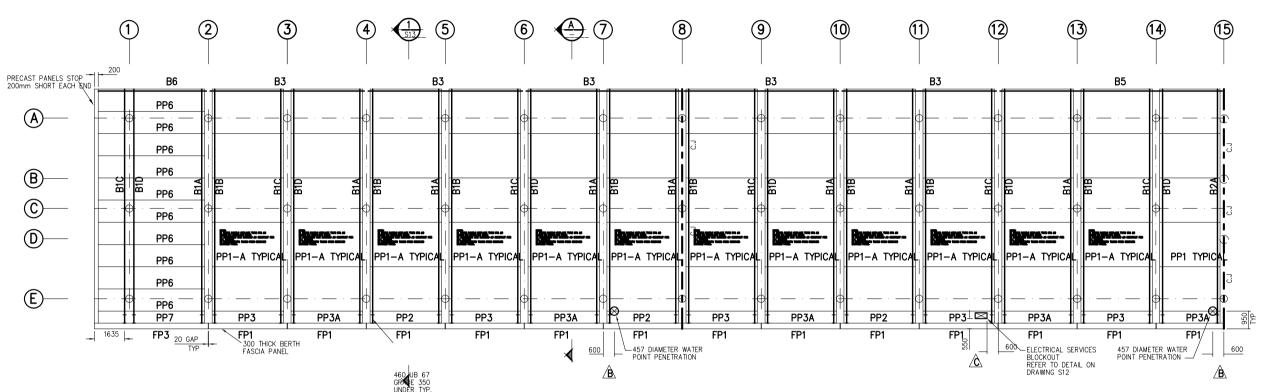
A3-



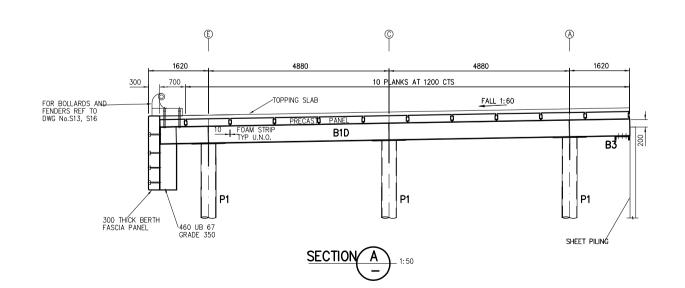




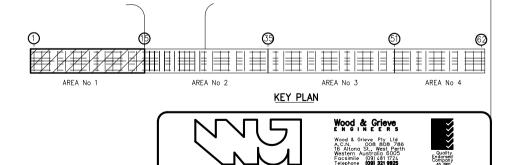
REV.	DESCRIPTION	APP'D	DATE
Α	ISSUED FOR APPROVAL	C.J.B.	23/11/94
В	GRID AMENDED & PENETRATIONS ADDED	C.J.B.	31/ 1/95
С	ELECTRICAL BLOCKOUT ADDED	C.J.B.	10/ 6/95
D	PANEL PP1-A TO REPLACE PP1	GMH/CR	15-10-08











CLIENT: GERALDTON PORT AUTHORITY

PROJECT: GERALDTON HARBOUR No 6 BERTH

PRECAST CONCRETE PANELS AND STEELWORK PLAN AREA 1

DESIGNED: TLF VERIFIED: // DRAWING NO. REV.

DRAWN: KM APPROVED // APPROVED FOR CONSTRUCTION: //

